



Advancements in Geopolymer Concrete Technology: A Comprehensive Review of Fresh, Hardened and Microstructural Properties

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ABSTRACT

This review summarizes recent developments in geopolymer concrete technology, focusing on fresh, hardened, and microstructural properties. Key findings include the impact of ultrafine ground granulated blast furnace slag on enhancing workability and reducing setting times. Geopolymer concrete exhibits lower density and improved water resistance compared to traditional concrete, with compressive, flexural, and split tensile strengths increasing over time. Microstructural analyses highlight denser matrices and improved mechanical properties through effective activation processes. These advancements highlight geopolymer concrete's potential as a sustainable and durable construction material, emphasizing the need for further research and development for widespread adoption in the industry. The review categorizes frequently employed precursors based on their primary chemical components and explores how different binder types impact various aspects of lightweight geopolymers. Additionally, it consolidates optimal mix designs from various studies to aid readers in

choosing suitable binders and achieving desired density and compressive strength goals through the utilization of different precursors, alkaline binder solutions, and lightweight concrete.

Keywords: FA, GGBS, Workability, Durability, Geopolymer and Microstructure.

ABBREVIATION

Abbreviation	Material Described
FA	Fly Ash
GGBS	Ground Granulated Blast Furnace Slag
CBA	Clay Brick Aggregate
RCA	Recycled Concrete Aggregate
PA	Pumice Aggregate
HCFA	High Calcium Fly Ash
LCFA	Low Calcium Fly Ash
BA	Bottom Ash
CDW	Construction and Demolition Waste

1. Introduction

1.1. Overview

Lightweight concrete is a rigid material with a lower density than regular aggregates such as sand, clay, and gravel, resulting in less dead-load while keeping acceptable strength. Its strength varies depending on the type and quantity of aggregate used, contributing to sustainable construction requirements. The emergence of lightweight aggregates, manufactured during the nineteenth and twentieth centuries, signalled a significant milestone in the advancement of lightweight concrete technology Mousa et al., (2018); Shahrour & Allouzi, (2020). Coarse aggregates for concrete production typically consist of crushed natural rocks or stones. Different regions, depending on their geological makeup, utilize different types of natural rocks such as limestone, basalt Shahrour & Allouzi, (2020). To tackle the aforementioned challenges, three technological approaches are proposed. These include aggregates recycled from waste concrete Akhtar & Sarmah, (2018); Dimitriou et al., (2018); Liu et al., (2020); Pawluczuk et al., (2019), repurposing coarse waste aggregates such as large-particle bottom ash and steel slag, and creating artificial aggregates using industrial wastes or by-products Qian et al., (2020); Tajra et al., (2019). Among these approaches, the artificial manufacturing method is gaining prominence as it offers a viable solution for producing both fine and coarse aggregates, meeting the demands of waste recycling and large-scale production. Presently, the primary focus lies on research into artificial coarse aggregates, spurred by the need to address shortages in fine aggregates through alternative solutions like the utilization of sea sand Huang, Weng, et al., (2021); Huang, Wu, et al., (2020); Huang, Yu, et al., (2020). Two well-established methods for manufacturing artificial

lightweight aggregates are sintering and cold bonding Qian et al., (2020); Tajra et al., (2019). Sintering predominantly depends on high temperatures, often exceeding 1000°C, to crystallize the precursors. Conversely, the conventional cold-bonding technique typically employs cementitious pastes for bonding the raw materials together. Geopolymer concrete demonstrates outstanding performance, including comparable mechanical strength, minimal shrinkage, excellent resistance to creep, and high durability even in acidic environments Reddy et al., (2016). Numerous factors influence the properties of recycled aggregate concrete, including the quality and quantity of recycled aggregate, water-to-cement ratio, mixing techniques, additives, and supplementary materials Guo et al., (2018); Li et al., (2016). Furthermore, recent investigations have focused on improving the properties of recycled aggregate to promote its utilization Dimitriou et al., (2018); Li et al., (2016). Each year, the global production of CDW amounts to around 820 million tons Gálvez-Martos et al., Mani & Pradhan, (2020). In the United States alone, approximately 500 million tons of CDW is yielded annually Akhtar & Sarmah, (2018), while China produces about 200 million tons. Recycling CDW presents a highly effective solution to these challenges. Aside from the expenses associated with waste disposal and the negative impact on landscapes, reusing these materials can mitigate issues like illegal dumping, which pose both social and environmental concerns Agwa et al., (2020). Raw materials can be natural resources such as perlite or pumice, or manufactured aggregates such as polyethylene particles, which are best acquired from trash or industrial byproducts to reduce quarry consumption Erfanimesh & Sharbatdar, (2020); Wang et al., (2020).

Ordinary Portland Cement (OPC) is often the primary binder for lightweight concrete, although it raises environmental problems due to CO₂ emissions and habitat destruction from material extraction Pratap et al., (2023). Zero-cement binders, such as geopolymer materials derived from waste aluminosilicates such as slag and fly ash, provide a greener alternative by creating geopolymers when mixed with chemical solutions such as sodium hydroxide Payakaniti et al., (2017). It is increasingly common to mix soils with processed rubber particles in various civil and geotechnical constructions, such as lightweight backfill Rouhanifar et al., (2021). Incorporating fiber into soil enhances both its shear and tensile strengths, while also increasing the material's ductility. Additionally, fiber-mixed soil exhibits a higher permeability coefficient and reduced swelling potential. Despite substantial research on geopolymers, there are few detailed studies of the mix design and attributes of lightweight geopolymer concretes. Microstructural analysis is also used to determine the durability and thermal qualities Nuaklong et al., (2019); Shi et al., (2020).

Geopolymers are moving beyond straight cement replacements, finding specialized uses in thermal and sound insulation where lightweight variations thrive. The review classifies commonly used precursors according to main chemical components and analyses how binder type influences various aspects of lightweight geopolymers. Furthermore, it combines optimal mix designs from numerous research to assist readers in selecting appropriate binders and reaching desired density and compressive strength targets using various precursors, alkaline binder solutions, and lightweight concrete.

1.2 Economic feasibility

Even though geopolymers are made from waste materials and have many desired properties, they are generally more expensive than normal OPC concrete. Geopolymer concrete can often be twice as expensive as regular concrete. This cost disparity is because of the large investment in manufacturing technologies and established infrastructure acquired over time for typical OPC concrete, which results in lower overall prices Carreño-Gallardo et al., (2018). Geopolymer concrete, as a relatively new technology, lacks manufacturing efficiency and infrastructure, contributing to its higher costs. However, as additional research and technologies are developed, the cost of geopolymer concrete (GPC) is expected to fall.

Analysing the cost breakdowns of conventional and geopolymer concrete yields intriguing findings. In traditional concrete, cement typically accounts for the majority of construction expenditures. Geopolymer concrete, on the other hand, has significantly lower costs for binders and aggregates because geopolymer binders are generally made from industrial waste materials Tayeh et al., (2021). However, alkali activators are important in geopolymer concrete and can significantly affect building costs. The development of cost-effective technology for producing alkali activators and binders like sodium silicate (SS) and sodium hydroxide (SH) has the potential to drastically reduce the overall cost of geopolymer concrete, making it more competitive with conventional choices Pratap et al., (2024).

In some areas, quality fly ashes and slag are mainly available but are being depleted due to stop of coal-fired power plants and reduce of blast furnace operations Hu et al., (2019). Such shortages may cause variations in GPC properties hence limiting its large-scale production. The chemical composition of fly ash and slag varies widely depending on their source causing variation in the performance of geopolymer concrete. The quality and consistency of these materials are fundamental for reliable performance characteristics of GPC. However, high-quality fly ash and slag are available only in certain parts of the world and can significantly differ according to local industrial activities Gartner & Sui, (2018).

Another important hurdle against the widespread use of geopolymer concrete is its production cost. Although GPC could be cheaper than PCC due to lower energy requirements as well as using industrial waste products, the prices for alkalis activators like sodium hydroxide or sodium silicate may be extraordinarily high sometimes Nematollahi et al., (2016). In addition, since GPC production processes are not fully developed compared to that of conventional concrete, expenses incurred when obtaining materials or ensuring the quality of materials are higher, including specialized machines needed. This variation between costs becomes more obvious when large-scale building projects are considered where the economy is always important.

1.3 Geopolymer concrete vs emerging alternatives

The most promising aspect of geopolymer concrete is its potential application to significantly cut carbon emissions compared to conventional concrete, using industrial byproducts like fly ash, slag, and

metakaolin. It enables low-carbon construction activities, associated with a shallow carbon footprint. Similarly, it is highly resistant to chemicals, fire, and attainable temperatures, making it ideal for infrastructures under adverse environments. However, geopolymer concrete is one of the mix designs that require stringent control in the mix and casting process; in most cases, it requires heat curing to reach its optimum. This can limit its widespread adoption, particularly in regions where these conditions are difficult to maintain.

Another promising alternative is alkali-activated materials, which include geopolymers as one of the groupings under its subset Pratap et al., (2023). AAMs give a flexible composition of binder; thus, a greater variation of industrial byproducts can be used as precursors to this class of materials. It is this versatility that AAM can adapt to various local resources and environmental conditions; it also provides high early strength and durability, equal to geopolymer concrete. Similar to geopolymers, the use of alkali activators can induce complexities in the mixing and handling processes Pratap & Kumar, (2023). In addition, problems in sustainability are sometimes created with the AAMs through the use of alkali activators, which are considered special in nature, both in type and source.

The other innovative approach to sustainable construction is carbon-sequestering concrete. This is a material manufactured with the specific purpose of capturing and storing carbon dioxide during the curing process, which effectively reduces the overall carbon footprint of the concrete. Some carbon-sequestering concretes use basically just a combination of Portland cement and alternative binders, while others may ditch cement completely for such things as magnesium oxide, which naturally absorbs CO₂. The main advantage of carbon-sequestering concrete is active removal, in the contribution to driving down atmospheric CO₂ concentration for battling climate change. The technology is, however, immature, and a host of problems—like scalability, cost, and variability in performance with respect to traditional and other alternative concretes—continue to loom large Pourjahanshahi et al., (2023).

In bio-based concretes, materials such as hemp, bamboo, or mycelium enable genuinely new avenues for building ecologically. As such, these materials are renewable, biodegradable, and can potentially have a much lower environmental impact than their counterparts of traditional cement-based products. However, in comparison, the compressive strength is lower than that of geopolymer or traditional concrete; thus, the use is limited to non-structural or low-rise buildings. The replacement materials make geopolymer concrete a good combination with optimum performance and the least possible environmental impact. Its performance shows the greatest impact in sections requiring durability and bearing the tendency to survive under extreme conditions. Indeed, the main barriers to its implementation are practical challenges like the necessity of precise mix control and heat curing.

On the other hand, AAMs are versatile and could be adapted to local conditions more, even though they face some difficulties with geopolymers that are similar in nature. Concretes sequestering carbon represents a solution that holds promise for strong environmental benefits, but is still on the developmental path. Lastly, bio-based concretes are green solutions for only a handful of niche markets right now, as they have yet to be optimized for large-scale production. Ultimately, the material selection

will be based on specifications within the project regarding environmental goals, service loads, and the availability of resources from regions with different climates. Geopolymer concrete, with superiority in sustainability and performance, depends on overcoming the associated technical challenges in its production and use.

2. Materials

2.1 Precursors

The production of Al-Si and Ca-Si materials involves distinct chemical processes, which has led to the differentiation between terminology such as "geopolymer" and "alkali-activated material". Traditionally, materials like Ground Granulated Blast Furnace Slag and fly ash are grouped under the geopolymer classification, whereas precursors derived from slag are typically termed as alkali-activated materials. However, recent studies have started using the term "geopolymer" inclusively for both groups, distinguishing between calcium-based and alumina-based geopolymers. Within concrete mixtures, geopolymers act as binders, offering the possibility to partially or completely replace traditional cement. Key chemical components essential for their formation include Silicon Dioxide (SiO_2), Aluminium Oxide (Al_2O_3), Iron Oxide (Fe_2O_3), and Calcium Oxide (CaO). These elements play pivotal roles in the molecular structure and binding properties of geopolymers. The combination of these chemical insights underscores the fact that precursor materials for geopolymer production exhibit a wide range of compositions, characterized by varying proportions of SiO_2 , Al_2O_3 , Fe_2O_3 , and CaO . Understanding the composition of each precursor material is paramount for optimizing geopolymer formulations. This understanding enables researchers and engineers to tailor the properties of geopolymers to suit specific applications, particularly as replacements for cement in concrete. By manipulating the composition of precursor materials, researchers can fine-tune the performance characteristics of geopolymers, enhancing their durability, strength, and other desirable attributes in concrete structures. Thus, a thorough comprehension of precursor composition serves as a foundational step in the advancement and widespread adoption of geopolymers as sustainable alternatives to conventional cement-based materials.

The reaction mechanism in geopolymers occurs in three main phases: (a) The breakdown of aluminosilicate into aluminate and silicate compounds, (b) condensation of the monomers (initiation of setting time), and (c) monomers polymerizing into an amorphous inorganic polymer. The alkali in cement activates GGBS particles, leading to the formation of its hydration products. The hydraulic properties of GGBS arise from chemical reactions between calcium, silica, and aluminium, which react with water to create calcium silicate and calcium aluminate hydrates. Some of these GGBS hydration products further react with Portland cement, forming additional hydrates that help block pores, resulting in a cement paste with very fine gel pores. This process enhances the stability of the hardened cement paste by reducing the free lime content Saranya et al., (2018).

This review aims to analyze the use of lightweight aggregates in geopolymer concrete, exploring their impact on durability, microstructure, and sustainability. It also investigates different methods for producing lightweight aggregates and their effects on concrete properties. However, there's a gap in understanding the mix design and attributes of lightweight geopolymer concretes, as well as a lack of systematic analysis of binder types and precursors. This review seeks to address these gaps by synthesizing existing research and providing insights for optimizing mix designs and selecting suitable materials for lightweight geopolymer concrete applications.

2.1.1 Fly Ash

Fly ash is a fine powder residue that is produced when coal is burned in power plants Xu et al., (2021). Fly ash and bottom ash are residues or secondary products that are produced when coal is burned, and they need to be disposed of in an environmentally friendly way Öz et al., (2021). The Mae Moh thermal power plant in northern Thailand produces about 3.0 million tons of lignite fly ash per year, which has a high silica and alumina content, making it suitable for utilization as a pozzolanic material in concrete as well as a foundational material for creating geopolymer binders Wongsu et al., (2016). Type F fly ash was characterized with a higher concentration of SiO_2 , Al_2O_3 , and Fe_2O_3 , total 79.49% Nuaklong et al., (2021). The fly ash comprising 45.23% SiO_2 , 19.94% Al_2O_3 , 13.15% Fe_2O_3 , and 15.5% CaO , it was classified as a Class C fly ash Posi et al., (2013, 2015, 2016).

2.1.2 Ground Granulated Blast Furnace Slag

GGBS is a by-product of iron production in blast furnaces, processed into a fine powder form by rapid quenching with water. Because of its superior cementitious qualities and advantages for sustainability, it is a supplemental cementitious material that is widely utilized in buildings. GGBS enhances concrete durability, reduces heat of hydration, and mitigates environmental impact by reducing CO_2 emissions associated with cement production. Its incorporation in concrete contributes to improved strength, workability, and resistance to sulphate and chloride attacks, making it an essential component in modern construction practices. In the study by Xu et al., (2021) the primary constituents of both GGBS and cement included SiO_2 , Al_2O_3 , and CaO . However, in comparison to GGBS, cement possessed a higher concentration of CaO and lower levels of SiO_2 and Al_2O_3 . Additionally, GGBS exhibited a predominantly amorphous phase Tayeh et al., (2021). In the study by Hu et al., (2019) GGBS was employed as a partial substitute for fly ash. The proportion of particles retained on the 45-micrometer sieve was 2.0%.

2.1.3 Bottom Ash

Bottom ash is a byproduct of burning coal in power plants. It consists of heavy particles that sink to the bottom of the combustion chamber. Bottom ash contains minerals like silica, iron, and aluminium, and is often reused in construction materials such as concrete and asphalt. Its disposal requires careful management due to potential environmental impacts. Wongsu et al. (2016) used the bottom ash (BA) Upon receipt, the BA was crushed and sieved to produce fine bottom ash (FB) and coarse bottom ash

(CB), which were utilized in the production of light weight geopolymer concrete (LWGC). The bottom ash proved suitable for application as both fine and coarse aggregates in high-strength concrete.

2.1.4 Recycled Concrete Aggregate (RCA) and Construction and Demolition Waste (CDW)

RCA and CDW play crucial roles in sustainable construction practices. RCA is derived from crushed concrete, offering a sustainable alternative to traditional aggregates, and reducing the need for fresh materials and landfill waste. CDW encompasses various materials generated during construction, renovation, or demolition activities, including concrete, bricks, wood, and metals. By recycling CDW and utilizing RCA, construction projects can minimize ecological footprints, preserve natural resources, and principles of circular economy.

Considering that coarse and fine aggregates typically constitute 75–80% of the overall concrete volume, the integration of C&D (Construction and Demolition) wastes, particularly in the form of recycled coarse aggregates (RCA), holds significant promise Shaikh, (2016). Within C&D materials, approximately 75% comprises concrete, while the remainder comprises masonry, tile, asphalt, and other components. The study by Rahman & Khattak, (2021) intended to introduce the idea of roller-compacted GPC in an effort to improve the mechanical properties of entirely recycled coarse aggregates (RCA). The loss on ignition (LOI) in CDW exceeds that of natural aggregates because of the presence of Portland cement and gypsum within the recycled aggregates Arenas et al., (2017).

2.1.5 Pumice Aggregate (PA)

Pumice Aggregate is a lightweight, porous volcanic rock used as an aggregate in construction materials such as concrete, plaster, and stucco. It is formed from volcanic eruptions and possesses excellent insulation properties, making it suitable for lightweight concrete applications. PA reduces the overall weight of the concrete while maintaining strength, aiding in easier handling and transportation. Its porous nature also enhances drainage and reduces water absorption in construction projects. Volcanic pumice, characterized by its natural lightweight attributes and sponge-like structure, is found in granular form, which results from the rapid cooling of molten lava Wongsu et al., (2018). Pumice aggregate can be utilized as a lightweight aggregate in structural concrete, prepared by refining natural materials such as pumice, scoria, or tuff. However, in the case of LWGCs made with PA, the compressive strength was notably reduced, rendering it suitable for the production of concrete blocks.

2.1.6 Clay Brick Aggregate (CBA)

Clay Brick Aggregate (CBA) is a sustainable alternative to traditional coarse aggregates in concrete production. It involves crushing and recycling waste clay bricks to create aggregates for use in construction. CBA offers several benefits, including reduced environmental impact by diverting waste from landfills, lower production costs compared to natural aggregates, and improved thermal insulation properties in concrete structures. In an experiment by Wongsu et al. (2018) crushed clay brick and pumice LWGCs demonstrated superior heat insulation and fire resistance properties in comparison to GPCs containing natural aggregates.

2.2 Light Weight Aggregate

Lightweight aggregates are materials used in construction that are lighter in weight compared to traditional aggregates like gravel or crushed stone. These aggregates are typically derived from natural materials such as expanded clay, perlite, shale, or slate, or from synthetic materials like foamed blast furnace slag or expanded perlite. The primary advantage of lightweight aggregates is their reduced density, which makes them particularly useful in applications where weight is a concern, such as in the construction of high-rise buildings, bridges, and precast concrete elements.

Lightweight aggregates offer benefits such as improved workability, reduced dead load on structures, and enhanced energy efficiency. Additionally, their low thermal conductivity can provide insulation properties, making them suitable for applications where thermal performance is important. However, they may have lower strength compared to traditional aggregates, so careful consideration is needed in their selection and use in construction projects. Overall, lightweight aggregates play an important role in modern construction, offering versatility and sustainability in various applications.

2.2.1 Natural Aggregate

Natural lightweight aggregates, like expanded clay, shale, slate, and pumice, offer construction materials with low density. These substances undergo processes such as heating or expansion to achieve their lightweight properties. Widely used in construction, they reduce structural dead loads, provide thermal insulation, and ease handling during construction. Applications include lightweight concrete, fill materials, and insulation.

The study by Wongsu et al., (2018) utilized various materials, including crushed clay brick aggregate, pumice aggregate, and crushed limestone aggregate. The coarse aggregates used in this work by Tayeh et al., (2021) are local dolomite, leca, and pumice. Öz et al., (2021) used quartz aggregates of various diameters, serving as natural aggregates (NA) used in the production of concrete. Wongsu et al., (2016) used natural aggregates like sand and crushed limestone. The natural coarse aggregate utilized by Hu et al., (2019) was crushed basalt aggregate sourced from a local site. It possessed an irregular morphology characterized by sharp edges.

2.2.2 Artificial aggregate

Engineered materials called artificial lightweight aggregates are used in construction to lighten concrete without sacrificing structural integrity. LWAs are generally composed of fly ash, shale, or expanded clay and have good strength, low density, and thermal insulation qualities.

In the experiment by Posi et al., (2013) and Posi et al., (2016) recycled lightweight blocks were processed into different aggregate sizes: fine aggregate, medium aggregate, and coarse aggregate. These aggregates were categorized based on particle sizes ranging from 0.001 to 1.18 mm for fine aggregate, 1.18 to 4.75 mm for medium aggregate, and 4.75 to 12.5 mm for coarse aggregate. Recycled packaging foam used in the study by Posi et al., (2015) was sourced from discarded packaging foam of household

electrical appliances. Initially, the foam pieces, ranging from 3.0 to 4.0 cm, were manually broken down and further ground using a food blender. Subsequently, the crushed foam underwent sieving to achieve particle sizes ranging from 2.36 to 4.75 mm. Öz et al. (2021) also used cold-bonded light weight fine aggregates (LWFA) as artificial aggregate, employed together with quartz. Arenas et al., (2017) and Shaikh, (2016) used CDW as an artificial aggregate.

2.3 Alkali Mixture for Activation and Binding

Alkali activators, such as sodium hydroxide (SH), sodium silicate (SS), potassium hydroxide (KOH), and calcium hydroxide ($\text{Ca}(\text{OH})_2$), initiate chemical reactions with alumina, silica, and other compounds in geopolymer solutions. Sodium and potassium ions, in various forms like silicate, carbonate, and sulphate, are crucial in these reactions. These compounds release hydroxyl ions (OH^-), aiding the disintegration of aluminate and silicate compounds in geopolymer precursors like fly ash. Typically, a single type of hydroxide, mostly SH for convenience, is present in the activation solution. Sodium hydroxide (SH) and sodium silicate (SS) were utilized as alkaline activators for producing geopolymer binder by all the researchers and their proportions are given in Table 1 and Table 2 present the chemical composition of different materials.

Table 1. Proportions of alkaline solutions adopted by various researchers

Study	SS/SH Ratio
Wongsa et al. (2018)	0.5, 1.0, 1.5
Wongsa et al. (2016)	-
Shaikh (2016)	2.5
Öz et al. (2021)	2.5
Rahman and Khattak (2021)	1
Posi et al. (2015)	1
Posi et al. (2013)	1
Nuaklong et al. (2021)	0.60
Hu et al. (2019)	2.0
Arenas et al. (2017)	0.29
Posi et al. (2016)	0.33, 0.67, 1.0, 1.5, 3

Table 2. Chemical Composition of Light Weight Geopolymer Concrete

References	Contents	Fe ₂ O ₃	Al ₂ O ₃	K ₂ O	MgO	CaO	SiO ₂	TiO ₂	P ₂ O ₅	SO ₃	BaO	LOI	Na ₂ O
Xu et al., (2021)	FA	9.19	26.9	1.28	3.49	9.14	43.4	0.91	0	1.65	0	2.9	3.16

Xu et al., (2021)	GGBS	0.27	16	0.43	8.69	39.9	31.1	0.72	0	2.44	0	2.71	0
Wongsa et al., (2018)	FA	11.5	20.8	2.4	2.2	14.5	39.4	0.5	0.2	4.2	0	1.5	1.4
Wongsa et al., (2018)	CBA	5.1	15.2	1.5	1.2	0.6	67.9	0.8	0	0	0	0	0.8
Wongsa et al., (2018)	PA	4	16.7	3.4	0.9	2.4	60.4	0.5	0.2	0	0	0	4
Shaikh, (2016)	FA	12.48	25.56	0.7	1.45	4.3	51.11	1.32	0.885	0.24	0	0.57	0.77
Tayeh et al., (2021)	FA	3.95	28.78	1.33	1.18	2.46	55.57	0.21	0	0.37	0	0.97	0.72
Tayeh et al., (2021)	GGBS	0.95	15.56	0.41	5.78	41.23	31.79	0.88	0	2.86	0	0.51	0.39
Rahman & Khattak, (2021)	FA	12.17	14.82	1.59	0.79	13.87	36.4	0	0	0.57	0	0	0
Rahman & Khattak, (2021)	RCA	12.96	2.52	0.9	0.4	59.68	17.78	0	0	0.76	0	0	0
Öz et al., (2021)	FA	7.02	22.2	2.34	1.7	1.47	61.3	0.9	0	0.06	0	2.6	0.27
Nuaklong et al., (2021)	HCFA	11.9	19.9	2.4	1.9	14.2	36.2	0	0	3.6	0	0.4	0
Nuaklong et al., (2021)	LCFA	2.9	25.8	1.8	0.5	4.2	60.6	0	0	0.4	0	2.3	0
Wongsa et al., (2016)	FA	11.5	20.8	2.4	2.2	14.5	39.4	0.5	0.2	4.2	0.1	1.5	0
Wongsa et al., (2016)	BA	18	12.1	2.5	2.4	25.3	31.8	0.5	0.3	3.7	0.2	3.2	0
Arenas et al., (2017)	FA	5.86	21.5	1.67	1.84	3.94	63.9	0	<0.01	<0.01	0	3.32	0.68
Arenas et al., (2017)	CDW	3.54	9.57	1.87	2.45	17.9	57.8	0	0.11	0.42	0	9.19	0.61
Posi et al., (2016)	FA	13.15	19.95	2.15	2.02	15.5	45.23	0	0	0.3	0	0.88	0.52

3. Mix Design

Optimal mix designs for various geopolymer concrete with lightweight aggregates are outlined in this review paper. The emphasis is on formulations with superior compressive strength and reduced densities. Components such as binder type and content, alkali activators, lightweight aggregates, curing conditions, and densities are highlighted. This information provides valuable insights for researchers and practitioners seeking to optimize mix designs for lightweight geopolymer applications.

3.1 Mixing

Geopolymer concrete production starts with mixing the alkaline activating solution and binding precursor, initiating chemical reactions to form gels and polymers. Aggregates are then added, and the mixture is poured into moulds, covered to prevent moisture loss. Subsequently, samples cure in ovens, controlled rooms, or both successively. Geopolymer pastes were made using one-part technology, dry-mixing precursors and alkaline activators for 5 minutes. Water was added for a duration of three minutes due to quick setting. Mixture cast into 100 mm × 100 mm × 100 mm moulds, covered, demoulded after 24 hours at 25°C. Eight specimens per mix proportion were prepared for future casting Xu et al., (2021). Fly ash and Superplasticizer (SH) mixed for 5 minutes, then aggregates for 2 minutes. Silica Fume (SS) added and mixed for 1 minute. Fresh mixtures compacted in moulds on a vibrating table for 10 seconds. Cylindrical samples with 10 cm diameter and 20 cm height cast for compressive and splitting tensile strength tests Wongsa et al., (2018). The study examines four mix series: GPC0 (control) with 100% NCA, and three others with 15%, 30%, and 50% RCA replacing natural coarse aggregates (NCA). Alkali activator to fly ash ratio is constant. Conventional mixing includes dry-mixing aggregates, adding class F fly ash, pouring alkali solutions gradually until uniformity is achieved visually Shaikh, (2016).

For Lightweight Oil Well Cement, cement, fly ash, and GGBS are mixed dry for 1 minute, followed by 2 minutes of fine and coarse aggregate mixing. Water and superplasticizer are gradually added over 2 minutes. In LWGC, solid components and aggregates are dry-mixed for 3 minutes, while liquid materials including sodium silicate, sodium hydroxide, and superplasticizer are premixed and added for 3 more minutes Tayeh et al., (2021). LWGC and conventional geopolymer concrete (CGC) were mixed at 25°C. FA and SH were mixed for 5 minutes, then aggregates for 2 minutes. SS was added for 1 minute. After 8 minutes, fresh concrete was tested for slump, cast, and compacted. Samples: Cylindrical (100 × 200 mm) for strength tests, plates (150 × 150 × 60 mm) for abrasion resistance, cubes (100 × 100 × 100 mm) for conductivity and ultrasonic pulse velocity (UPV) tests Wongsa et al., (2016). Figure 1 shows the cast cylinders of GPC concrete with CDW Arenas et al., (2017).



Figure 1. Geopolymer concrete specimens

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3.2 Curing Procedure

Beam specimens measuring 100mm x 100mm x 400mm were prepared using the mould. Using a vibratory hammer and top plate, the mixture was crushed inside the mold. Following compaction, the specimen was taken out of the mold, sealed appropriately, and then put in an oven to cure at a high temperature Rahman & Khattak, (2021). For a full day, the GPCs were cured at 100°C in the oven. Once the samples had cured, they were removed from the molds and stored at room temperature until they were old enough to be tested Öz et al., (2021). Figure 2 shows the cast specimens of concrete cured at elevated temperatures Rahman & Khattak, (2021).

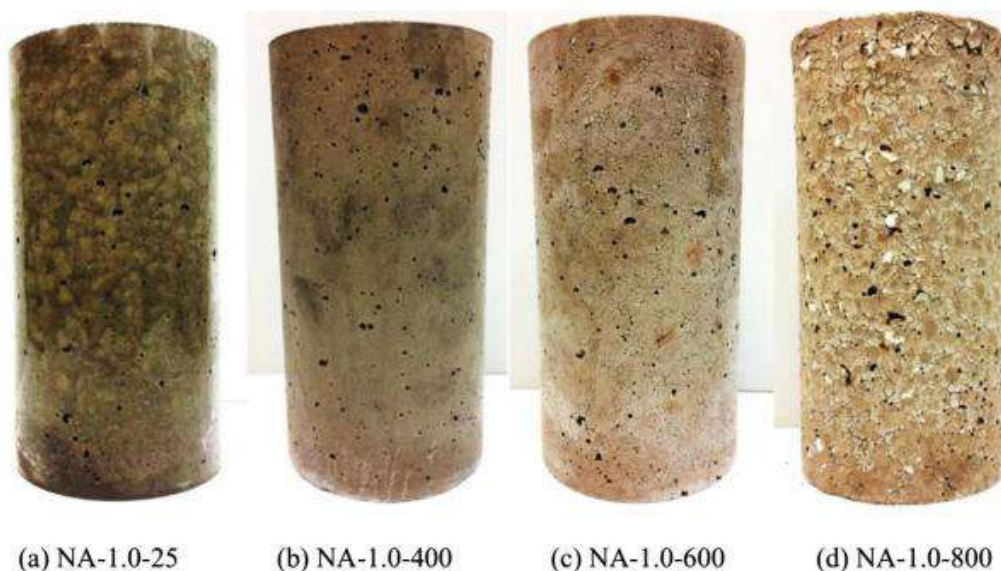


Figure 2. GPC specimens after exposure at 25°C, 400°C, 600°C, and 800°C

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After casting, GPC is steam-cured for 24 hours at 60°C. Specimens cure under standard circumstances following demoulding and before testing. Durability properties are examined on day 28, although

mechanical properties are studied at days 7 and 28. Concrete cylinders measuring 200 mm in height and 100 mm in diameter have compressive strength and elastic modulus, and indirect tensile strength is measured by those with a 150 mm diameter and 300 mm height Shaikh, (2016). For compaction, the freshly mixed material was put into moulds and set on a vibration table. After that, specimens were shielded from evaporation throughout the curing process with a thin layer of plastic film Hu et al., (2019). A little increase in compressive strength was observed when the temperature was raised from 25 to 90°C. This increase was ascribed to improved geopolymerization and the creation of more byproducts Posi et al., (2016).

4. RESULT

4.1 Fresh Properties

4.1.1 Workability

Workability is a key property of concrete, indicating its ease of handling and placement. It is influenced by various factors and ensures that concrete can be effectively mixed, placed, and compacted without issues such as segregation or bleeding. Achieving the right workability is essential for constructing durable and high-quality concrete structures. PA particles' water content improved workability, raising concrete slump. LWGCs with coarse aggregate (CA) had lower slump than CGCs with natural aggregate (NA), due to rounder river sand particles compared to fine CA, despite similar shapes in crushed limestone and coarse CA particles Wongsa et al., (2018). The figure 3 below exhibits the variation in slump value for different SS/SH ratios as well as for various aggregates (NA, CA, and PA).

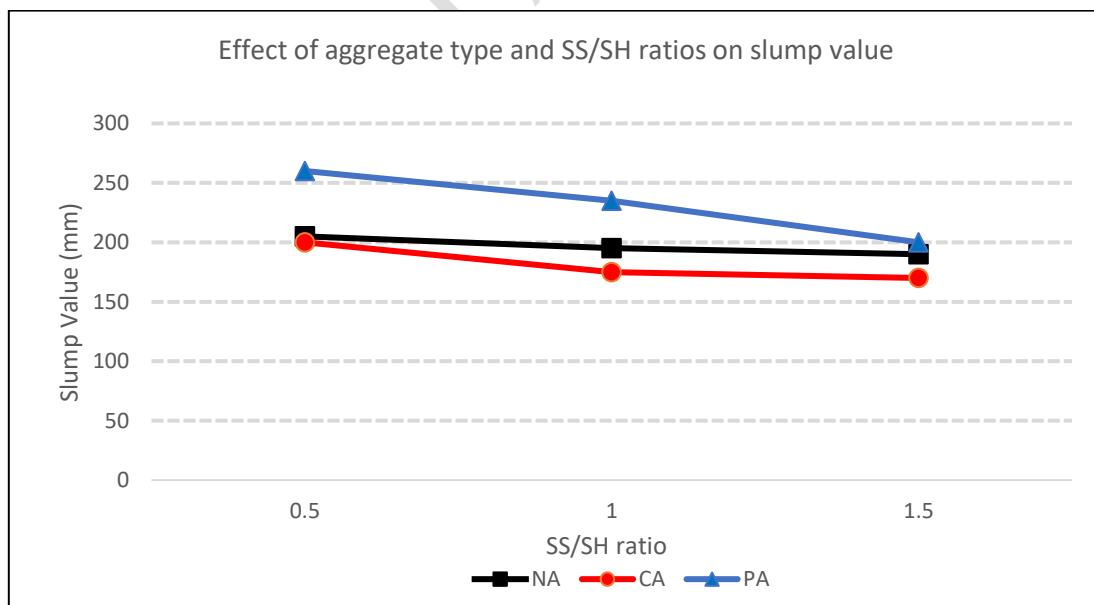


Figure 3. Effect of aggregate type and SS/SH ratios on slump value

GPCs had better workability than the control mix. The workability enhanced from 1.1% to 7.63% as compared to the control. Aggregate properties and binder components affect flowability. The rise in workability as compared to the control mix is shown in figure 4 Öz et al., (2021).

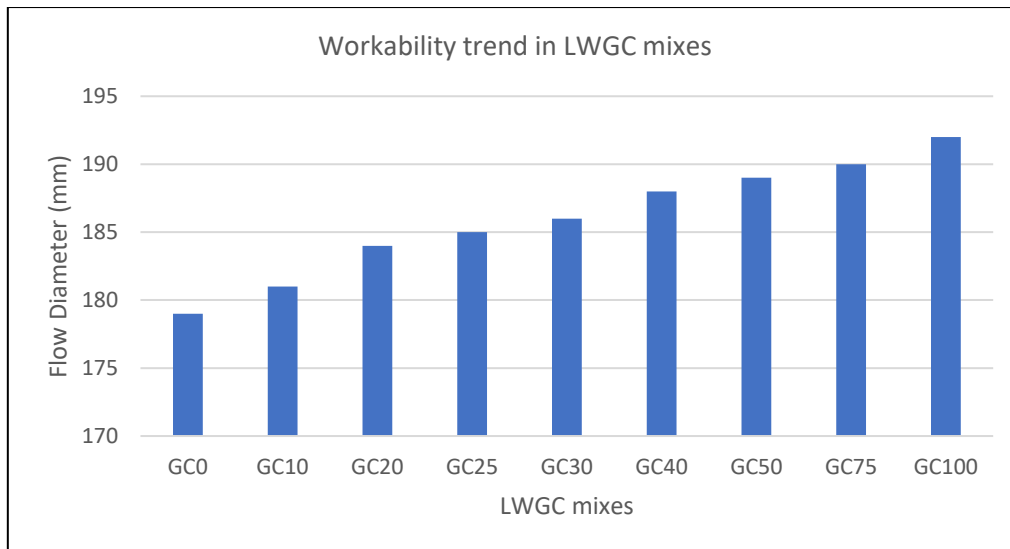


Figure 4. Flow diameter of various LWGC mixes

SS has a high viscosity and restricts mixture flow, higher SS/SH ratios reduced slump values Wongsa et al., (2016). Slump values significantly decreased as the amount of GGBS in the binder was increased, particularly at higher GGBS concentrations. The high calcium ion content dissolved from GGBS caused a quick reaction with the alkali activator, which precipitated as calcium silicate hydrate, which was the cause of this loss in workability. The mixes with higher slag content showed lower workability as compared to ordinary concrete (control mix). The trend in workability can be seen in figure 5 (Hu et al., 2019).

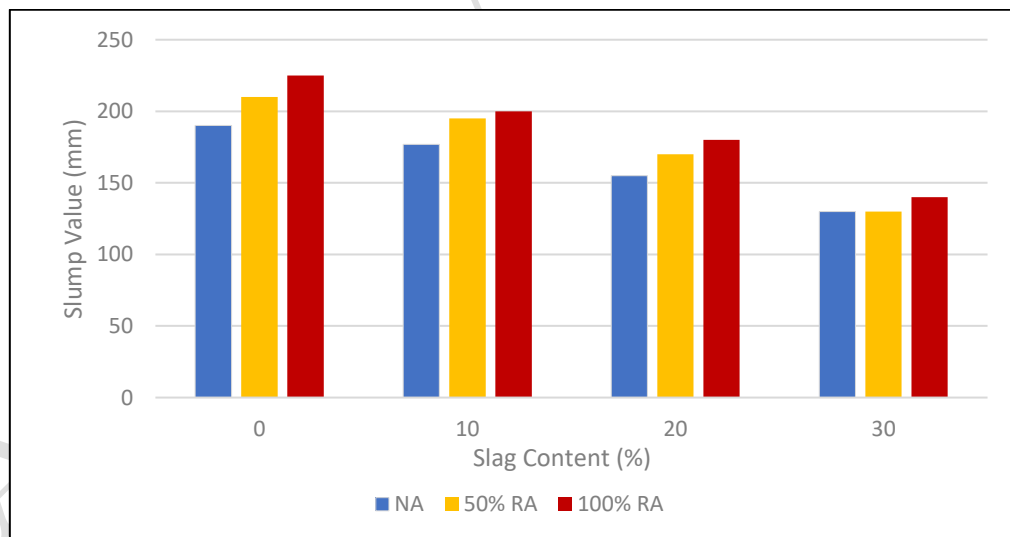


Figure 5. The trend in workability at various slag content

4.1.2 Setting Time

Setting time is the amount of time needed for a cementitious substance, such as mortar or concrete, to solidify and harden from a malleable, working state. It is a crucial characteristic influencing workability and building schedules. Temperature, admixtures, cement type, and water-to-cement ratio all affect setting times. Achieving the intended building results requires careful observation and management of

setting time. The crushing time may lengthen as the GPC setting time does, and vice versa. When GGBS is added (Group B) or the alkaline content is increased (Group A), the strength of the geopolymer mix increases Xu et al., (2021). High-calcium fly ash geopolymer sets quickly at low NaOH concentrations due to calcium leaching and precipitation, reducing workability and resulting in low density. Higher NaOH concentrations (10 and 15M) extend setting times, slightly improving workability and increasing concrete densities Posi et al., (2016).

The GGBS content primarily influenced the setting time of geopolymer composites. Mixtures without GGBS took a significantly longer time to set. However, the incorporation of GGBS in the binder considerably reduced both the initial and final setting times of the geopolymer composites. Additionally, as the GGBS content increased, the setting time (both initial and final) consistently decreased as we can see in Figure 6 (Hu et al., 2019).

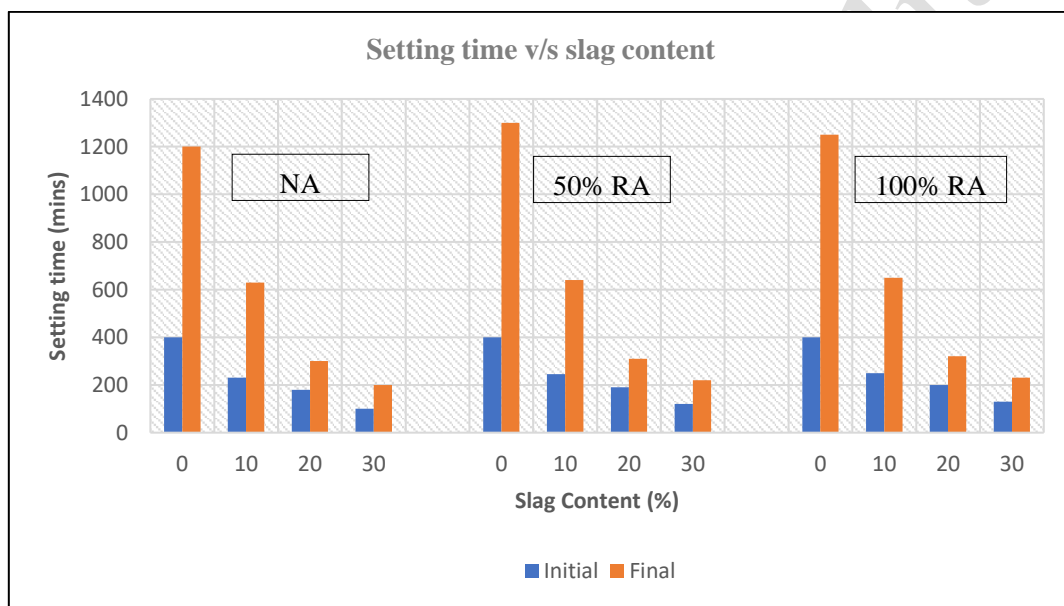


Figure 6. Setting time v/s slag content

4.1.3 Density

The loss of density was experienced in LWGCs with PA as compared to those that had either CA or NA. At temperatures of 400°C, 600°C, and 800°C for instance, the PA-1.0 samples lost their density by 24%, 29%, and 31% respectively. CA-1.0 samples also had lower reductions than PA-1.0 samples too but to smaller degrees: 14%, 17%, and 18%. The corresponding losses for NA-1.0 were 5%, 6%, and 7%. The reason behind this greater loss in PA is due to higher water absorption which leads to more mass loss resulting into lower compressive strength at high temperatures Wongsa et al., (2018).

Table 3. Density of various samples

Sample ID	Density (kg/m ³)
NA-1.0-25	2339
NA-1.0-400	2212
NA-1.0-600	2162

NA-1.0-800	2099
CA-1.0-25	1961
CA-1.0-400	1700
CA-1.0-600	1652
CA-1.0-800	1638
PA-1.0-25	1357
PA-1.0-400	1079
PA-1.0-600	1023
PA-1.0-800	1016

The as-cast surfaces of concrete blocks with OPC content (0%, 5%, 10%, and 15%) reveal that 0% OPC leads to low density due to the presence of a lot of voids. Addition of 5% and 10% OPC reduces voids and increases density, with 10% OPC achieving highest density and strength. Although, at 15% OPC, the mixtures became too dry resulting in rough surfaces that are less dense and strong. This is shown in Figure 7 (Posi et al., 2016).

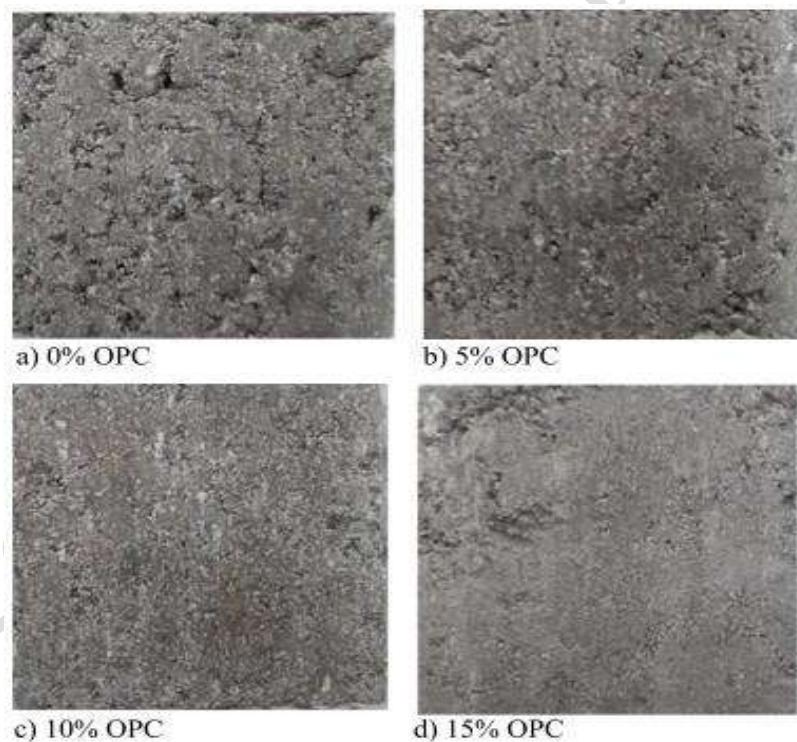


Figure 7. Cast surface of concrete for varying proportions of OPC content
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The density values fell between 2165 kilograms per cubic meter and 2432 kg/m³, depending on GGBS content as well as the recycled aggregate replacement ratio. Density was increased when fly ash was substituted with GGBS but decreased by 4-8% when using recycled aggregates due to its lower density Hu et al., (2019).

4.1.4 Segregation and Bleeding

Segregation and bleeding are common issues in concrete mixes. Segregation occurs when coarse aggregates settle and separate from the mortar, leading to uneven distribution of materials. Bleeding involves the migration of water to the surface due to the settling of heavier materials, leaving a layer of water on the surface. Both issues can compromise the strength and durability of concrete, leading to uneven surfaces and reduced quality. Proper mix design and handling techniques are essential to minimize segregation and bleeding and ensure uniform and durable concrete structures. No segregation or bleeding was observed in any of the mixes by any researchers.

4.2 Durability

4.2.1 Water Absorption

Water absorption refers to the process by which substances take in water molecules. In various contexts, water absorption plays critical roles, from biological organisms to industrial materials. In plants, water absorption occurs through the roots, facilitating nutrient uptake and supporting growth. In materials science, understanding water absorption is crucial for assessing properties like durability and permeability in construction materials or determining the efficacy of absorbent products like diapers. The phenomenon of water absorption underscores the fundamental role water plays across different domains of science and everyday life. Water absorption in geopolymer concrete rises with higher RCA contents, showing about 20% more absorption at a 50% RCA content. This aligns with sorptivity and is attributed to the greater absorption of water by RCA due to adhered old mortars, which are typically more porous than NCA Shaikh, (2016).

The water absorption rates of GPCs ranged from 7.5% to 11.2% at day 1, 5.6% to 9.4% at day 7, and 4.4% to 8.6% at day 28. Correspondingly, the apparent porosity values varied from 11.6% to 16.4%, 5.5% to 13.5%, and 5.3% to 6.6% for the same test ages, respectively Öz et al., (2021). Water absorption in LWGC slightly rose with higher aggregate/ash ratios. For instance, at 28 days, for 0F mixes with ratios of 2.0, 2.2, 2.4, and 2.6, absorption rates were 30.13%, 30.70%, 31.40%, and 32.15% respectively. Porosity followed a similar trend, increasing with higher aggregate/ash ratios Posi et al., (2013).

4.2.2. Chemical resistance

The research conducted by Shaikh, (2016) demonstrates that the partial replacement of grade coarse aggregates by RCA leads to considerable increases in chloride penetration in geopolymer concrete as observed from the GPC15, GPC30 and GPC50 series; 67%, 90% and 129% respectively from the initial control. Such low resistance may have been induced by water absorption and high porosity associated with it due to the permeable mortar attached to its surface and brick materials in it. GPC has been acknowledged to perform better than conventional PCC when subjected to harsh environments like industrial waste disposal sites, acid soils, and ocean waters Posi et al., (2015). The use of geopolymer binders that are low in calcium minimizes the formation of expansive substances like ettringite or

gypsum in sulphate attacks which are commonly seen in cement. Besides, this can also be explained by good chemical resistance resulting from dense microstructures that hinder the entry of harmful ions.

4.2.3. Freeze-thaw Resistance

Freeze-thaw durability is an important issue for concrete structures located in cold climates. This is so because GPC generally exhibits good freeze-thaw resistance as it has low water absorption and finer pore texture Huang, Wu, et al., (2021). However, the most reliable freeze-thaw resistance properties depend on the mix design including the type and amount of activators employed. Some researchers have observed that GPC activated by sodium silicate has better freeze-thaw resistance than GPC activated by sodium hydroxide due to the production of a more cohesive and less porous matrix.

4.2.4. Chloride Ion Penetration

The resistance of geopolymer concrete to chloride ion penetration is crucial in estimating its durability, especially in marine areas. Numerous studies indicate that GPC often presents a lesser degree of chloride penetration compared to normal concrete because it has a much tighter microstructure and lower volumes of empty spaces Öz et al., (2021). Nevertheless, employing the RCA as GPC components may lead to reduced resistance against chloride ions due to increased porosity and water usage within the RCA. Consequently, this calls for aggregate type selection and mix design which will ultimately improve GPC against attack by Cl ions.

4.2.5. Long-Term Durability

While there are not many long-term durability studies about geopolymer concrete, the studies that exist indicate that GPC can keep its mechanical properties and resistance to environmental degradation for a long time. Fly ash-based GPC, for instance, has shown little loss in strength and maintained its structural integrity after an extended time of exposure to severe conditions such as high temperatures and harsh chemicals Nuaklong et al., (2018).

4.3 Mechanical Properties

4.3.1 Compressive Strength

The fundamental mechanical characteristic of concrete is its compressive strength, which denotes its capacity to withstand pressure or axial stresses. Usually, it is assessed by compressing cylindrical or cubic specimens until they break. In order to evaluate the structural soundness and load-bearing ability of concrete in a variety of applications, such as infrastructure, buildings, and bridges, compressive strength is essential. It's common to need good mix design, high-quality materials, sufficient curing, and appropriate building techniques to achieve high compressive strength.

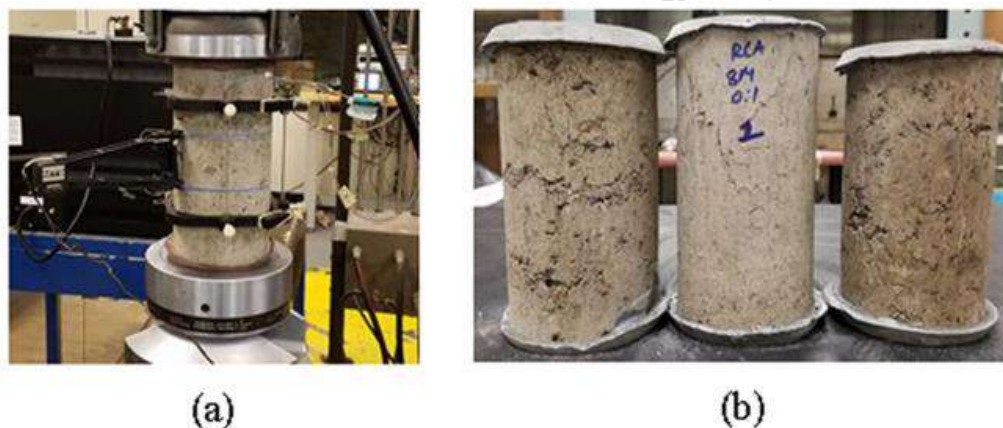
Among the various factors studied by Posi et al., (2013), the highest compressive strength of 15.4 MPa was achieved. NaOH solution concentration of 10M, higher curing temperatures up to 60°C, and lower aggregate/ash ratios for improved strength. Tayeh et al., (2021) found the following compressive

strength observations as specified in Table 4 on varying the various aggregate percentages in the concrete mix.

Table 4 Compressive strength of various concrete mixes on varying aggregate size

Concrete Mix	Aggregate Type	CS (28 Days) (MPa)
LWGC (Fly Ash)	100% Dolomite	58.1
LWGC (GBFS)	100% Dolomite	56.8
LWGC (Fly Ash)	50% Dolomite + 50% Leca	48.7
LWGC (GBFS)	50% Dolomite + 50% Leca	47.5

Rahman & Khattak, (2021) observed that increasing NaOH molarity from 6 M to 10 M in the GPC mixture with 100% RCA at 60°C significantly boosted both UCS (unconfined compressive strength) and E (modulus of elasticity). Mixtures with 8 M and 10 M NaOH saw UCS increases of 61% and 100% respectively compared to 6 M. This is due to increased OH production, vital for aluminosilicate gel formation and strength. The compression test and failed specimens are shown in Figure 8.



(a)

(b)

Figure 8. (a) Compression test (b) Failed GPC specimens

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Nuaklong et al., (2021) found that the use of carbon fibre (CF) resulted in increased compressive strength, likely due to enhanced matrix structure via micro-aggregate effect, leading to a more compacted microstructure. Beyond 1% CF content, there's a notable rise in the compressive strength of geopolymer mortar. Mixtures with 0.2% and 0.3% CFs exhibited 11-21% and 10-19% higher compressive strengths respectively. A graph of the compressive strength before and after exposure to temperatures of 400°C, 600°C, and 800°C observed by Wongsa et al., (2018) is provided in Figure 9. Posi et al., (2015) observed different trends in changing the concentration of alkali/ash ratio and SS/SH ratio and also the change in curing temperatures. The trends are shown in Figures 10a, 10b, and 10c.

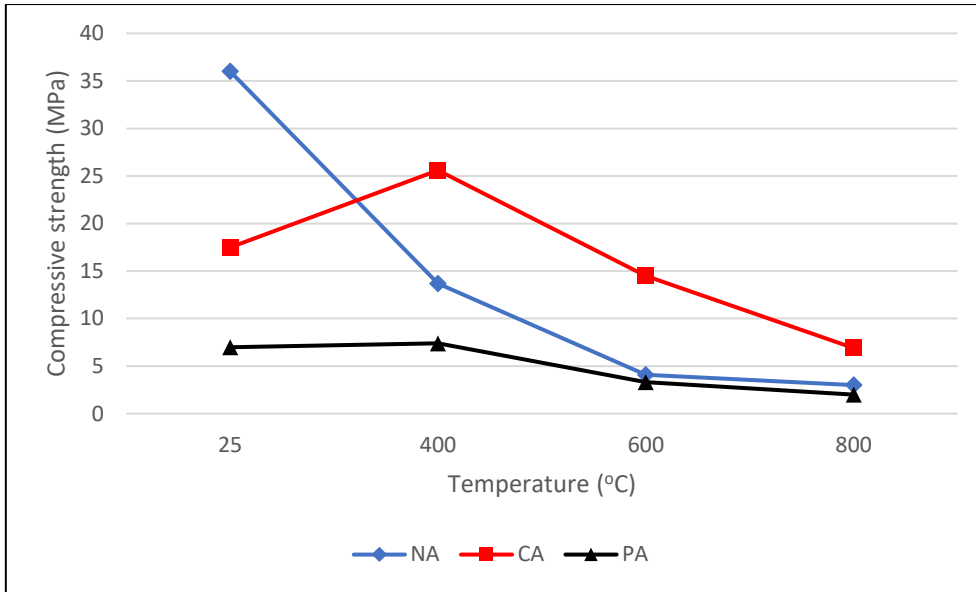


Figure 9. Effect of temperature on the compressive strength

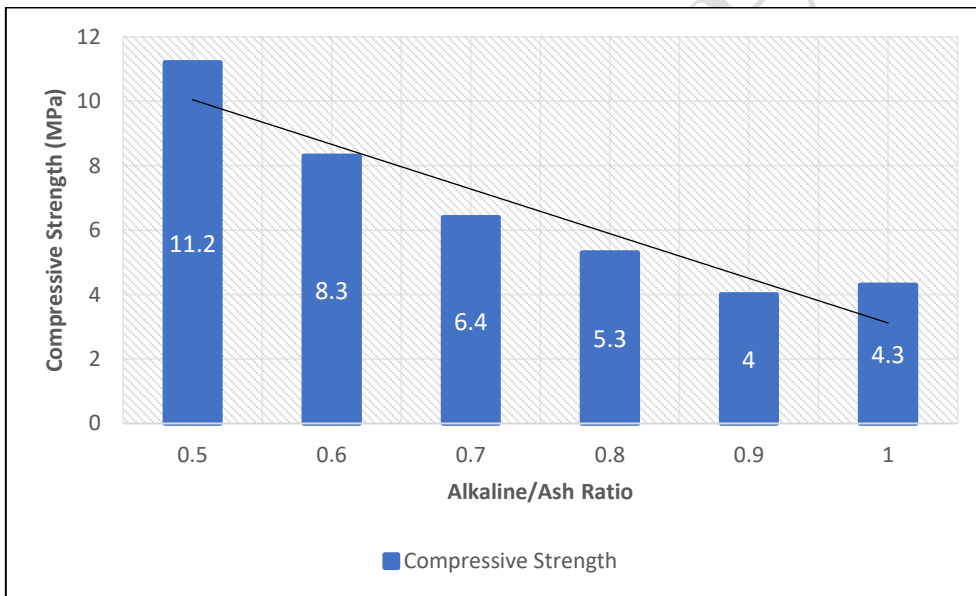


Figure 10a. Effect of alkaline to ash ratio on the compressive strength

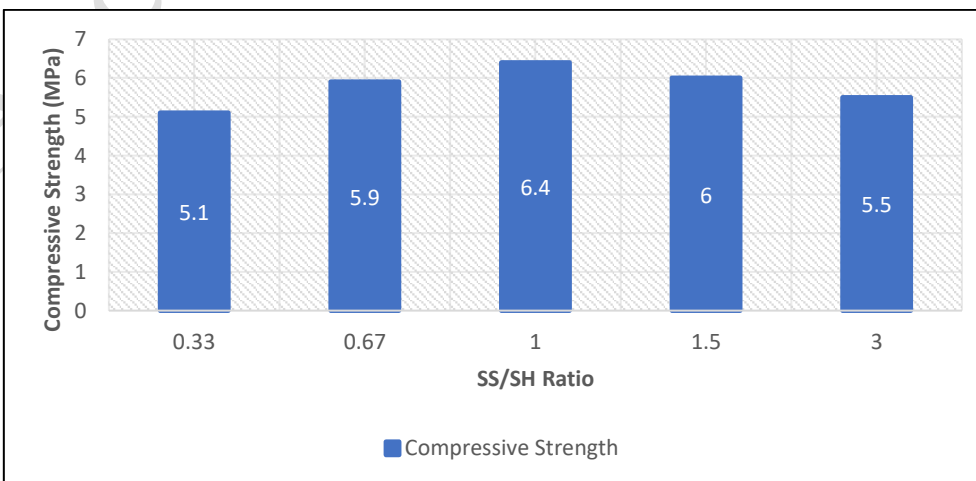


Figure 10b. SS/SH ratio effect on the compressive strength

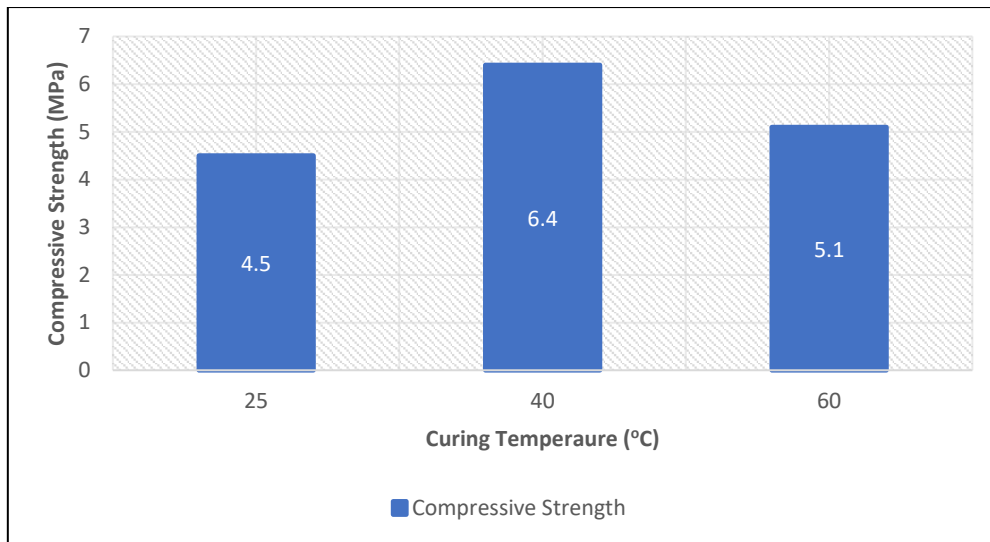


Figure 10c. Effect of different curing temperatures on the compressive strength

4.3.2 Flexural Strength

Flexural strength, also known as modulus of rupture, is a key mechanical property of materials, especially in engineering and construction. It measures a material's ability to withstand bending without breaking. For instance, in structural engineering, it's crucial for designing beams, columns, and other elements subject to bending loads. Materials like concrete, wood, and steel exhibit flexural strength, which is determined through standardized tests. Understanding flexural strength aids in optimizing designs, ensuring safety margins, and selecting appropriate materials for various applications. It's a fundamental parameter in ensuring the structural integrity and longevity of built environments. The use of light-density aggregates (Leca and pumice) in 100% proportion led to a decrease in density and flexural strength compared to other mixtures. Lightweight concrete (C-100-L and C-100-P) achieved lower flexural strength compared to conventional mixtures. Geopolymer concrete with light-density aggregates also exhibited lower density and flexural strength. The best FS for lightweight geopolymer concrete mixes (FG-50D50 L and FG-50D50 P) was achieved when combined with 50% fly ash and 50% ground blast furnace slag, with results of 7.18 MPa and 7.24 MPa, respectively, at the test age of 28 days Tayeh et al., (2021). The trend of FS of different mixes is shown in Figure 11 below.

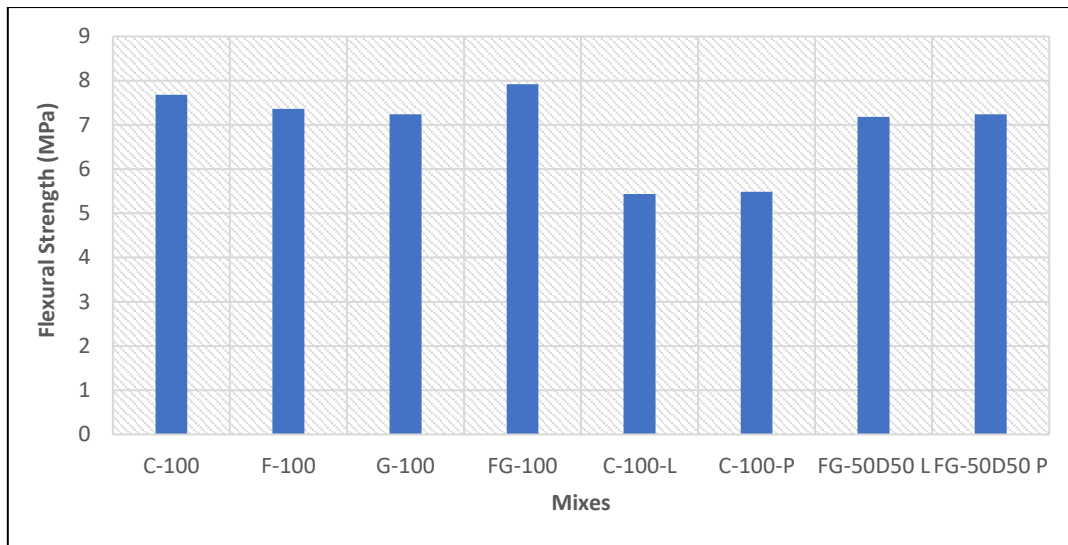


Figure 11. Variation in flexural strength

The study by Rahman & Khattak, (2021) found that the flexural strength (FS) of roller compacted geopolymer concrete (RCGPC) increased notably with the addition of alkali activators. Specifically, the inclusion of Na_2SiO_3 resulted in a substantial 40% enhancement in FS due to the improvement of the adhesion bond between recycle concrete aggregate (RCA) and the geopolymer matrix. Moreover, higher NaOH molarity further bolstered the FS, showing a significant 32% increase. RCGPC mixtures demonstrated superior FS compared to RCA conventional concrete mixtures, exhibiting up to a remarkable 71% improvement. Figure 12 shows the test for flexure along with the failed specimen.



Figure 12. (a) Flexure strength test (b) Failed specimen

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The FS test results of GPCs in the experiment by Öz et al., (2021) indicated that increasing the LWFA in the mixtures led to higher flexural strength. The optimal replacement level was found to be 25%, with minimal impact on FS observed at 30% and 40% replacement levels. However, higher replacement levels resulted in significant strength loss, with reductions of 16%, 23%, and 28% at 50%, 75%, and 100% replacements, respectively, after 28 days.

Flexural strengths of geopolymers increased notably with fibre addition, particularly at a carbon fibre (CF) content of 0.2%. This effect was more significant in mixtures made from recycled concrete aggregate (RCA). The maximum increase observed was 54% for the 100R-0.2CF composite compared to the unreinforced sample (100R mixture) Nuaklong et al., (2021). The variation in FS is shown in the figure 13 below.

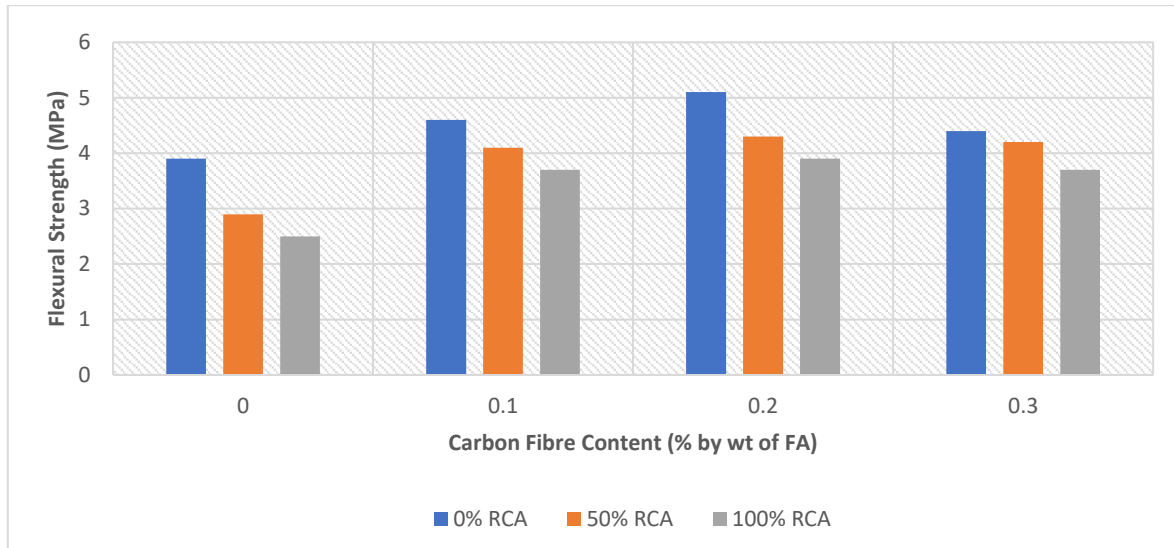


Figure 13. Variation in flexural strength due to change in fibre content

Mixtures with GGBS show significant strength improvements: up to 43% increase without recycled aggregate, up to 92% increase with 100% recycled aggregate. They also suffer less reduction in FS compared to those with FA alone, especially at higher recycled aggregate contents. Specifically, reductions in FS were less than 13% and 26% for mixtures with FA and GGBS at 50% and 100% recycled aggregate content, respectively, compared to 24% and 37% reductions for mixtures with FA alone Hu et al., (2019).

4.3.3 Split Tensile Strength

Splitting tensile strength measures a material's resistance to tensile stress applied perpendicular to its surface. It's crucial for assessing brittle materials like concrete or rock, often used in construction. This indirect testing method involves applying force diametrically to a cylindrical specimen until failure occurs, providing insights into a material's durability and performance. Replacement of natural aggregate (NA) with recycled concrete aggregate (RCA) decreased splitting tensile strength. The inclusion of 100% RCA reduced tensile strength from 2.6 MPa to 1.9 MPa. The addition of carbon fibers (CF) enhanced tensile strength, with a maximum increase of 38% observed in 50% RCA + 0.2% CF mixture. However, at 0.3% CF, the tensile strength slightly decreased compared to 0.2% CF, possibly due to improper fiber dispersion Nuaklong et al., (2021).

Table 5 tensile strength variation of different RCA

Mixture	Tensile Strength (MPa)
100% RCA (0R)	2.6 -> 1.9
50% RCA + 0.3% CF	-
50% RCA + 0.2% CF	38% increase
50% RCA + 0.1% CF	8% increase
50% RCA + 0% CF	No change

At 28 days, both cement concrete and geopolymer samples showed decreased tensile strength with lightweight aggregate use. Dolomite aggregate produced the highest strength. Lightweight concrete, C-100-L (Leca) and C-100-P (Pumice) had lower tensile strengths: 3.82 MPa and 3.74 MPa, respectively Tayeh et al., (2021). The splitting tensile strength of various mixes is shown in Figure 14.

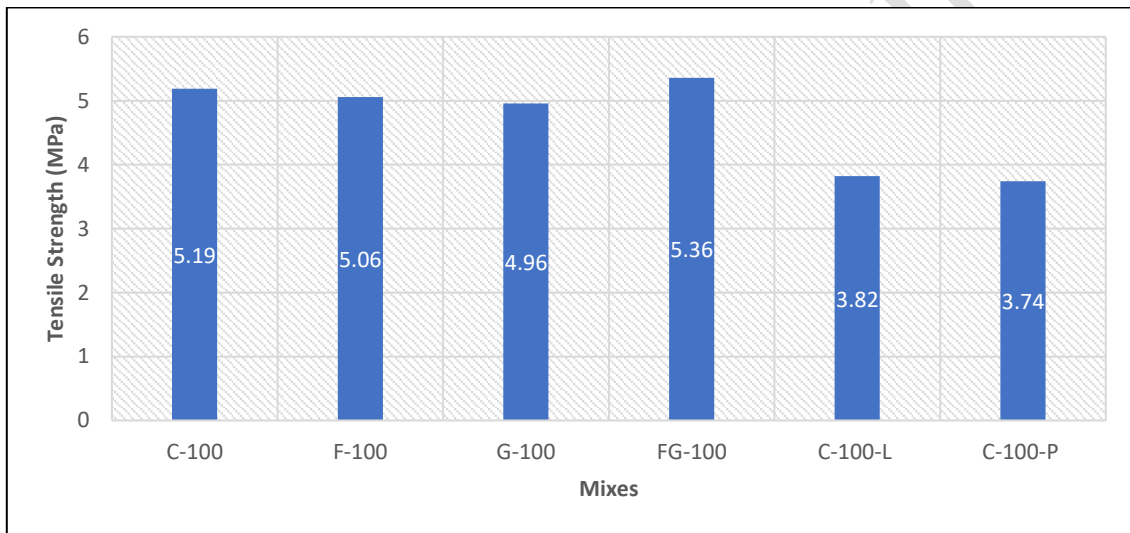


Figure 14. Splitting tensile strength of various geopolymer mixes

In this investigation by Wongsu et al., (2016), LWGCs showed an average splitting tensile to compressive strength ratio of 9.6%, higher than CGCs' 6.6%. In contrast to high-calcium fly ash geopolymer concrete, LWGCs with heat curing and comparable SH concentration had a higher ratio (9.6% vs. 6.9%). The range of stated values for conventional concretes (8 - 14%) was not exceeded by the splitting tensile to compressive strengths ratios for LWGCs (7.5 - 14%) and has been given in Table 6 (Wongsu et al., 2016).

Table 6. Ratio of Splitting Tensile to Compressive Strength (%)

Type of Concrete	Ratio of Splitting Tensile to Compressive Strength (%)
LWGCs (Lightweight Geopolymer Concrete)	7.5 - 14
CGCs (Conventional Geopolymer Concrete)	6.6
High-Calcium Fly Ash Geopolymer Concrete	6.9

4.4 Microstructural Characterization

4.4.1 SEM

Observing the surface appearance and structure of materials at high magnification is possible with the use of scanning electron microscopy (SEM), a potent imaging technique. SEM uses a concentrated electron beam to scan the surface of the sample, producing signals that can provide incredibly sharp, detailed images. Scanning electron microscopy is used to identify the microstructure, which shows the composition of two types of concrete: geopolymer concrete and regular concrete, which contains Portland cement with a weight ratio of 450 kg/m^3 .

As shown in Fig. 15a, partially dissolved cement grains exhibited several surface cracks, likely caused by the heat generated during cement hydration. This suggests that similar to traditional cement concrete, not all cement grains form calcium silicate hydrate (C-S-H) gel. In contrast, the microstructure of the geopolymer, depicted in Fig. 10b-c, reveals a typical SEM micrograph of a mix containing fly ash. The image shows geopolymer gel with partially or completely unreacted fly ash particles, along with the formation of pores and a heterogeneous matrix, which were not present in the original fly ash. This matrix formation resulted from the geopolymerization reaction that occurred after mixing the fly ash with the alkaline activator liquid Tayeh et al., (2021). The SEM images are shown in figure 15.

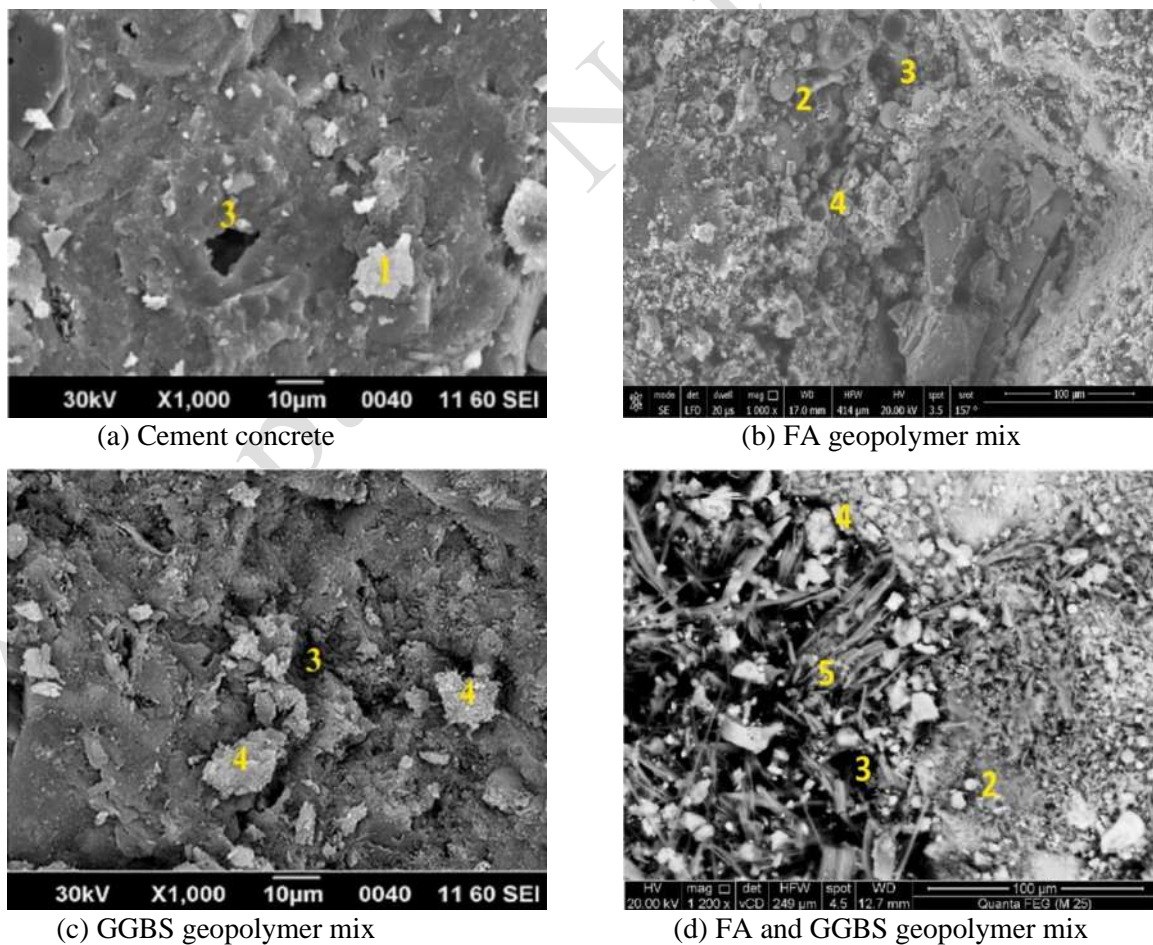


Figure 15. SEM images for conventional and geopolymer mix.
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SEM micrographs of the RCA-RCGPC mixture were examined, revealing the use of an 8 M NaOH solution as the activator (Figure 16). Within these micrographs, it was evident that some fly ash particles remained partially or wholly unreacted within the mixture. This presence of unreacted fly ash particles elucidates the comparatively lower strength of the mixture when compared to mixtures utilizing Na_2SiO_3 as an activator Rahman & Khattak, (2021).

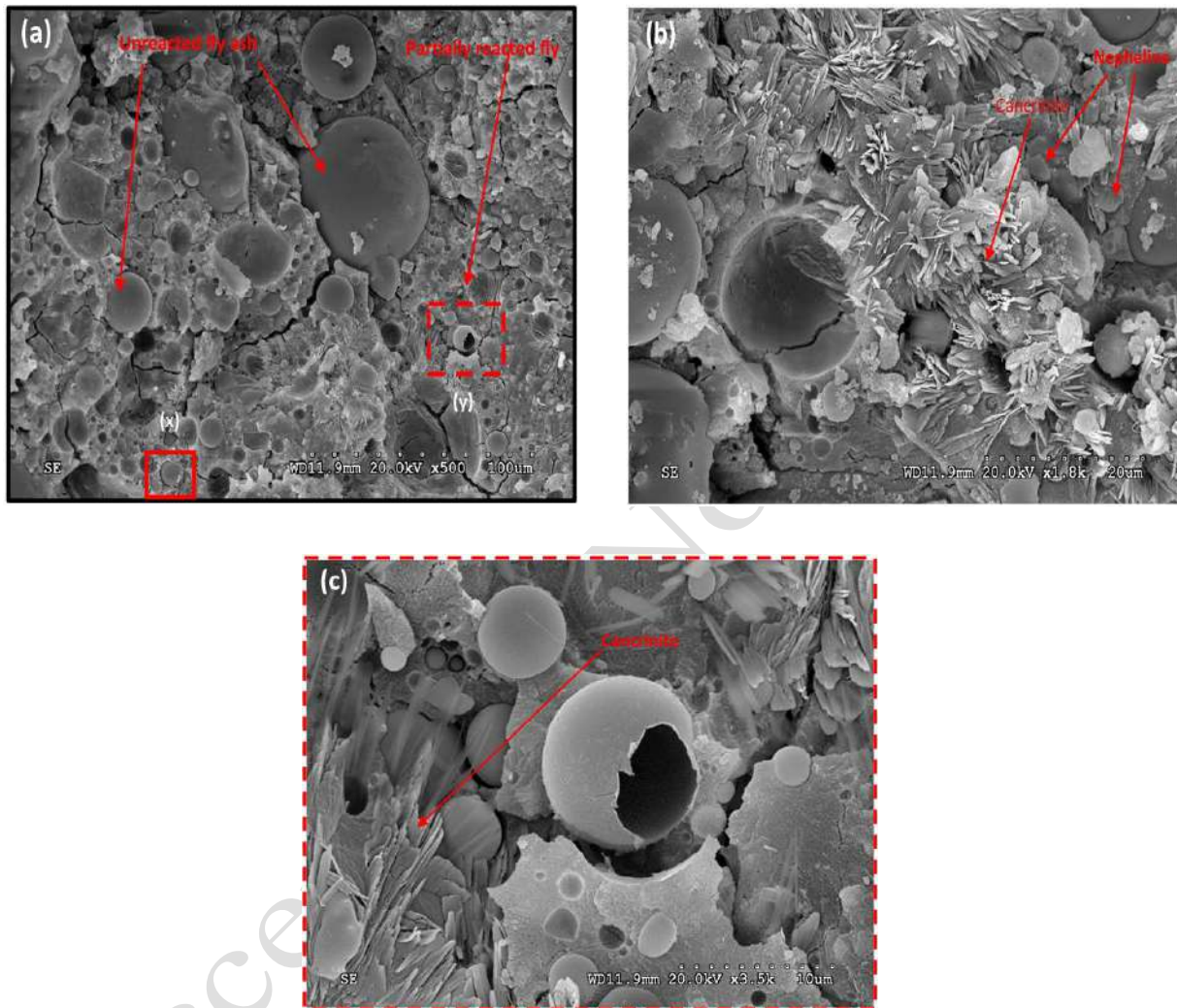
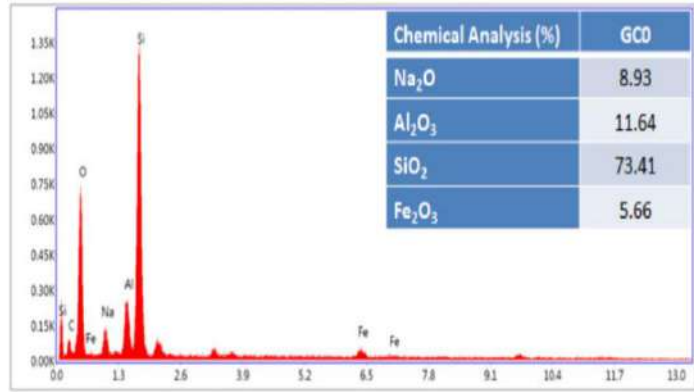
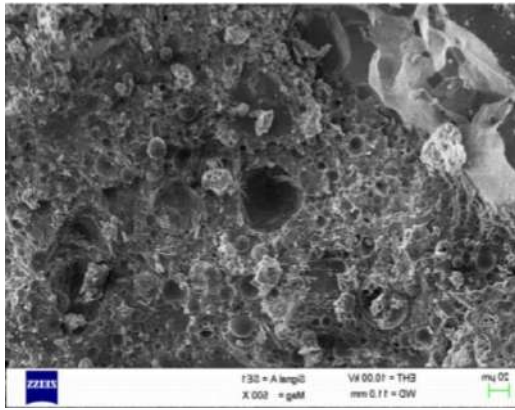
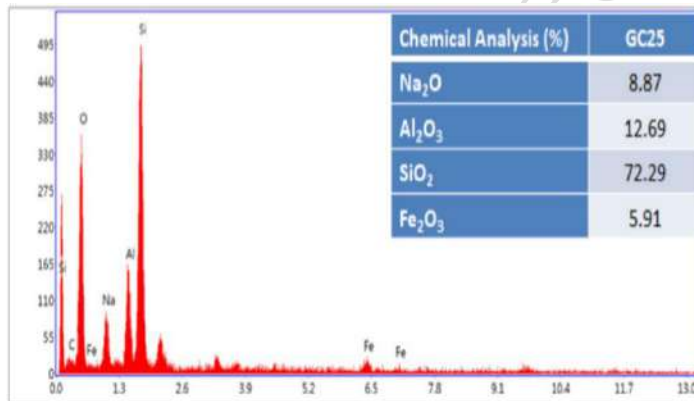
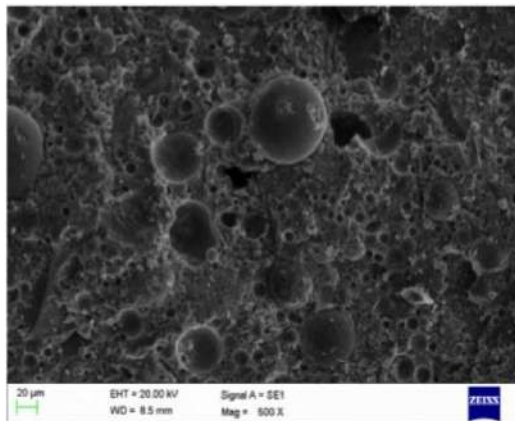


Figure 16. (a) SEM of RCA-RCGPC with 8 M NaOH cured at 600C. (b) zoomed image of "x" (c) zoomed image of "y"
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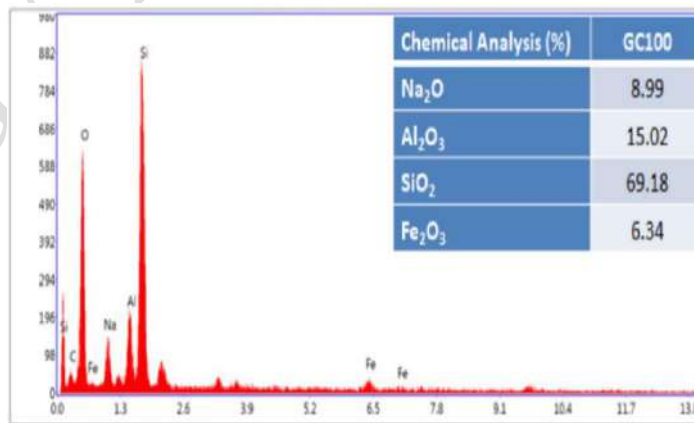
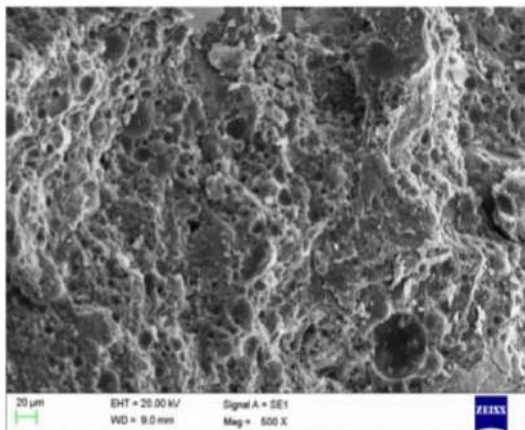
SEM analysis revealed distinctive morphological alterations in the GPCs. These changes are attributed to the predominant presence of Al and Si, derived from FA during alkali activation, which are the main constituents contributing to GPC gel formation. Additionally, the GPCs are composed mainly of Na_2O , Al_2O_3 , and SiO_2 , along with traces of Fe_2O_3 Öz et al., (2021). Images are shown in figure 17.



(a) GC100 (Control mix)



(b) GC 25



(c) GC100

Figure 17. SEM images of (a) GC0, (b) GC25, (c) GC100, and EDX results of (d) GC0, (e) GC25, (f) GC100.
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SEM images in figure 18 show unreacted fly ash particles hindering crack propagation in geopolymer pastes, though cracks may still occur due to increased stress. Carbon fibres (CF) act as micro-aggregates with minimal effect on crack resistance despite strong bonding, fiber fracture, and pull-out dissipate energy. As depicted in figures 18 a, b, c and d, both fiber fracture and fiber pull-out behaviours were observed. Fiber frocking is a clear sign of strong attachment between carbon fibre carbon composite and geopolymers. Therefore, it is likely that energy losses happened through the frictional movement of the fibers. A porous "fiber fossil" layer indicates pull-out under shear stress. Excessive carbon fibers

hinder the alkaline solution-fly ash reaction, potentially reducing SiO_2 and Al_2O_3 leaching in 0.3% CF-containing pastes Nuaklong et al., (2021).

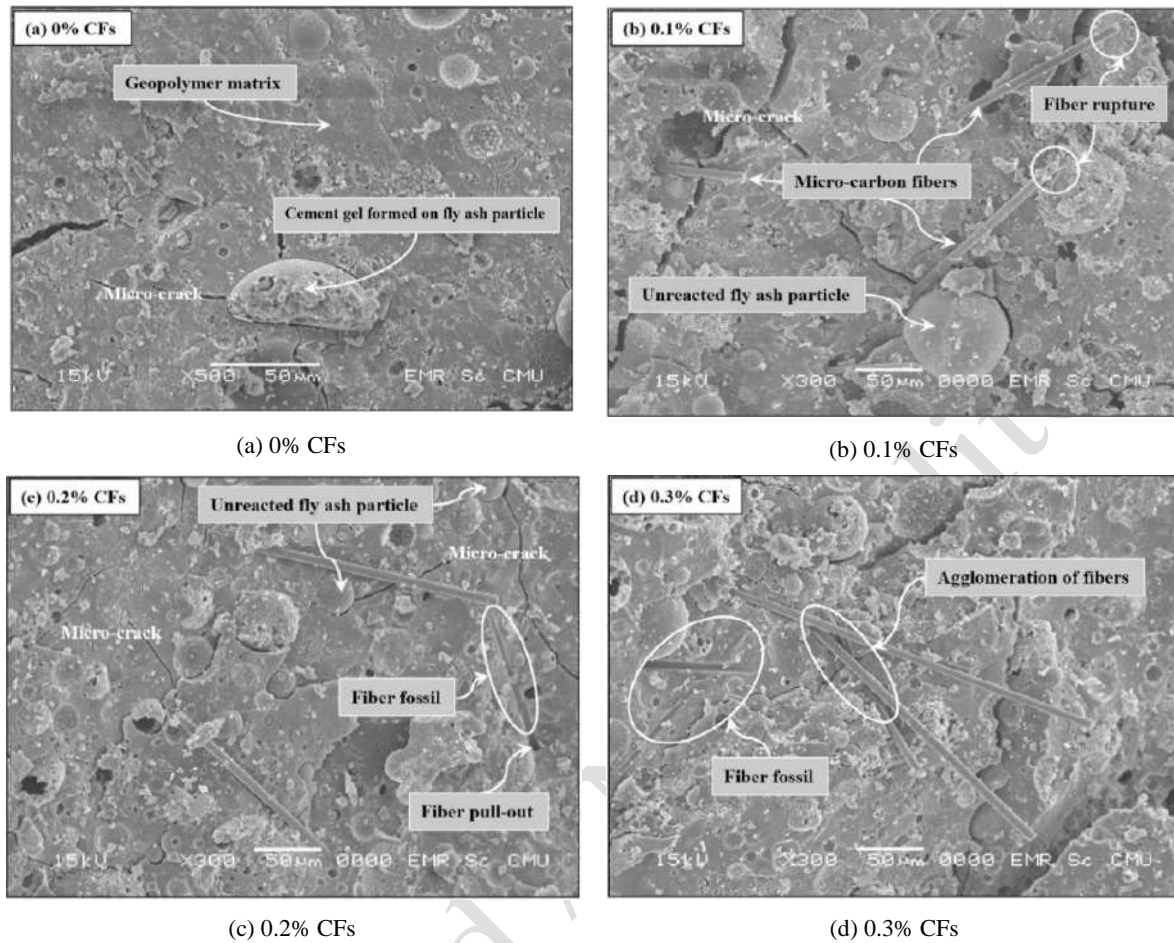
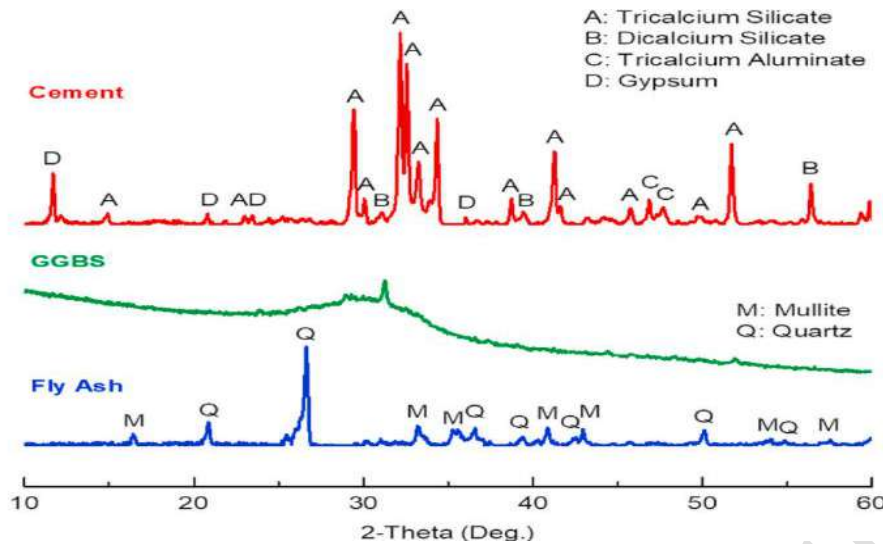


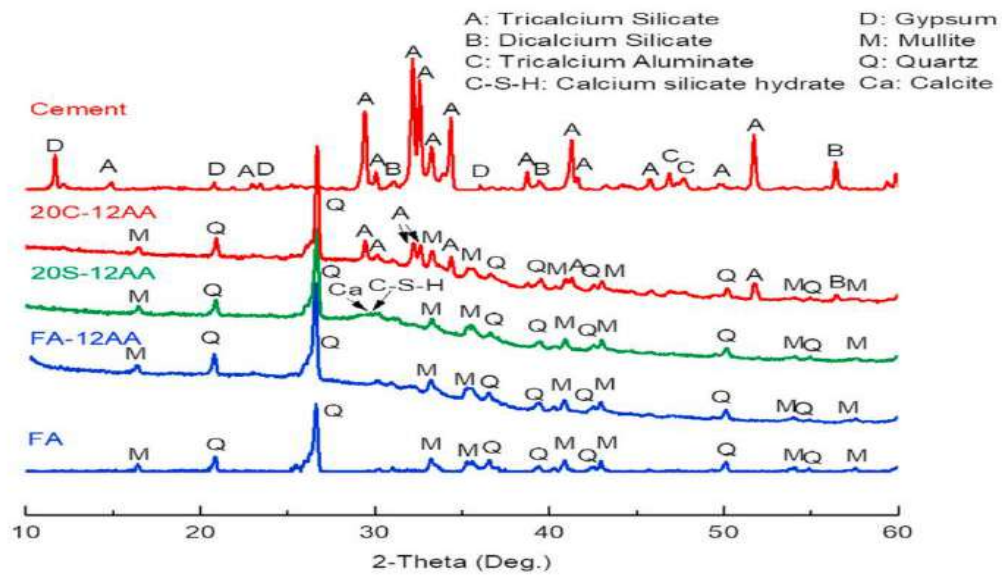
Figure 18 SEM image of geopolymer paste sample having (a) 0% CFs, (b) 0.1% CFs, (c) 0.2% CFs and (d) 0.3% CFs. " Permission and Rights have been taken from the publisher and its License Number—5776390408245 "

4.4.2 XRD

A non-destructive analytical method for determining a material's crystallographic structure is X-ray diffraction (XRD). An X-ray is utilized to bombard a material in an XRD test, and the diffraction pattern is analyzed. When X-rays interact with the sample's crystal lattice, constructive interference occurs at specific angles dictated by the lattice spacing, which leads to the development of this pattern. The preservation of quartz and mullite, which were previously present in FA and were not impacted by alkali activation, demonstrated the amorphous character of FA geopolymer products in figure 19 (Xu et al., 2021).



(a) XRD patterns of FA, GGBS and cement



(b) XRD patterns of GLAs at 28-day age

Figure 19. XRD patterns of FA, GGBS, cement and geopolymer light aggregates (GLAs).
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The XRD graphs showed unreacted quartz and mullite compounds, which was in line with the results of the XRD micrographs shown in figures 20 and 21. All of the mixture's Mullites reacted with 10 M NaOH to produce nepheline, syvatoslavite, and cancrinite, demonstrating a strong geopolymeric reaction. The aluminosilicate compounds were found to have lower peaks when NaOH was used as the only alkali activator Rahman & Khattak, (2021).

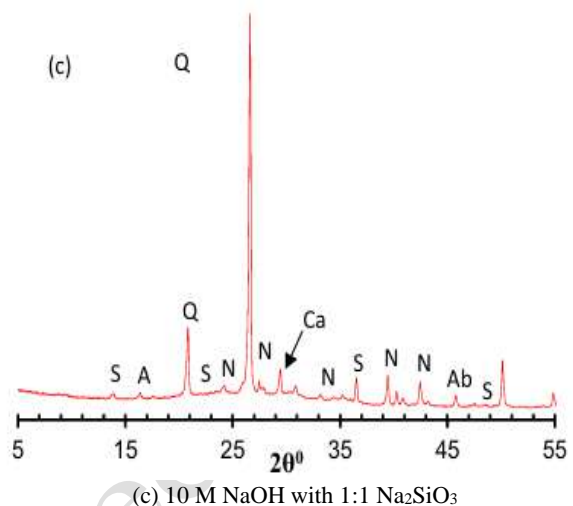
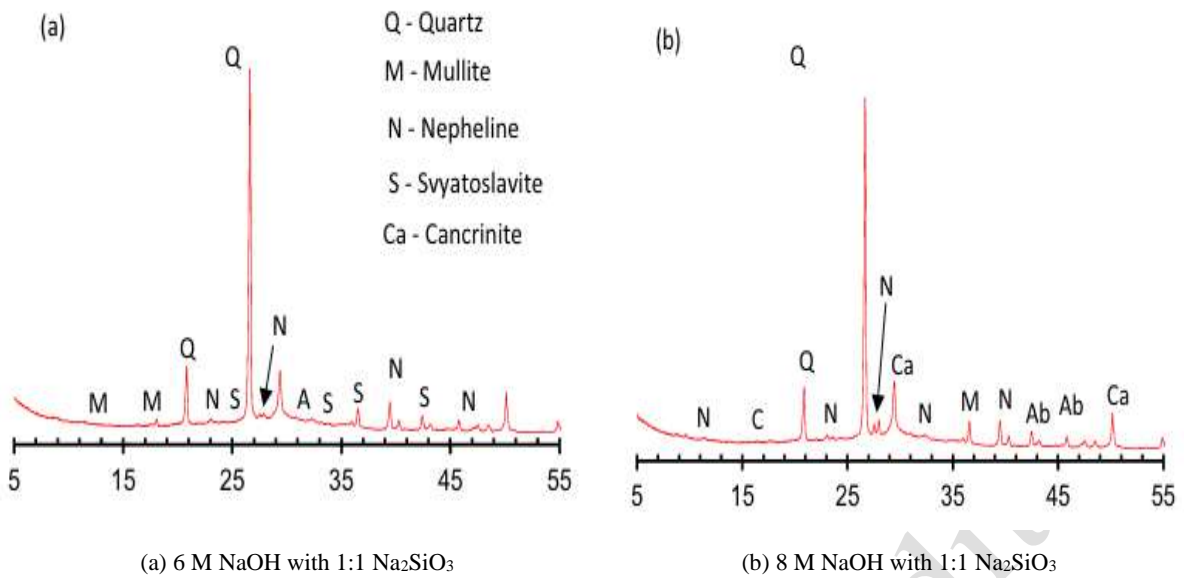


Figure 20, XRD of GPC mixes cured at 60 C.
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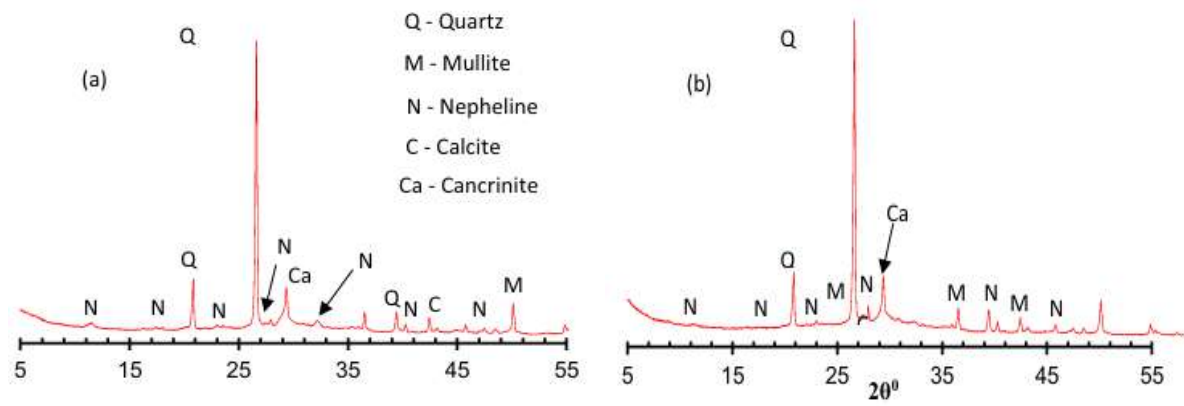


Figure 21 XRD of (a) 8 M NaOH cured at 60 C and (b) 8 M NaOH with 1:1 Na₂SiO₃/NaOH ratio cured at 25 C.
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In study by Öz et al., (2021) peaks for albite ($\text{NaAlSi}_3\text{O}_8\text{-A}$), nepheline ($\text{AlNaSiO}_4\text{-N}$), and hematite ($\text{Fe}_2\text{O}_3\text{-H}$) may be seen in the XRD patterns of GC0, GC25, and GC100, together with crystalline quartz ($\text{SiO}_2\text{-Q}$) and mullite ($\text{Al}_2\text{O}_3\cdot 2\text{SiO}_2\text{-M}$). These peaks show that Q, M, and H are present in the FA. Furthermore, the peaks for A and N show how FA reacts to activators in figure 22. The A and N peaks indicate that fly ash (FA) reacted with the activators. As shown in Fig. 22, the addition of lightweight fly ash (LWFA) to geopolymer concrete reduced the intensity of the Q peak. This is evident from the pronounced Q peaks at $21^\circ 2\theta$ and $26.8^\circ 2\theta$. The decreasing intensity of the Q peak with increasing LWFA can be attributed to the reduced presence of quartz sand, which has a high SiO_2 content. Despite the reduction in the Q peak, the increase in strength can be explained by the fact that FA-based LWFA plays a chemical role in the matrix, similar to that of FA.

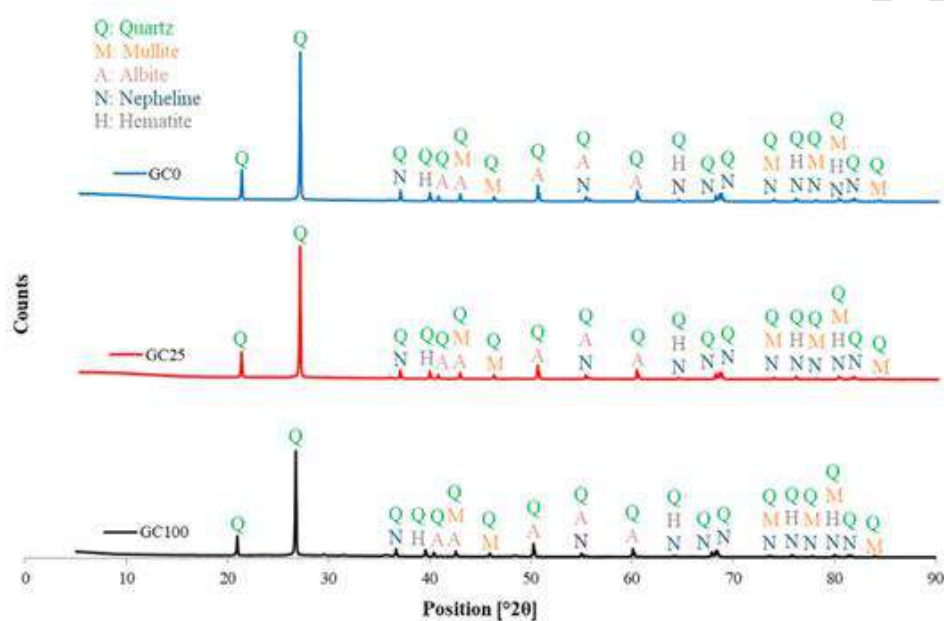


Figure 22. XRD patterns of GC0, GC25, and GC100.

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4.4.3 FTIR

FTIR stands for Fourier Transform Infrared Spectroscopy. It is an approach to determine a sample's molecular composition by measuring the amount of infrared light it absorbs. When infrared light interacts with a sample, certain wavelengths are absorbed, corresponding to specific vibrational modes of the chemical bonds within the molecules. By measuring which wavelengths are absorbed, FTIR can provide information about the functional groups present in the sample, helping to identify its chemical structure and composition. The spectra showed peaks at $3700\text{--}3400\text{ cm}^{-1}$ and $1700\text{--}1600\text{ cm}^{-1}$, indicating O–H stretching and H–O–H bending from water (H_2O) molecules formed during geopolymerization. O–C–O stretching at around 1400 cm^{-1} was observed, indicating sodium carbonate (Na_2CO_3) formation from reaction with CO_2 . Significant Si–O–T stretching occurred at $1200\text{--}950\text{ cm}^{-1}$, with increased intensity indicating higher geopolymerization. The mixes containing carbon fibers

showed a more pronounced Si–O–Si or Si–O–Al stretching peak compared to the control mixture. Although carbon fibres are chemically inert, they likely act as a dispersion agent, helping to de-agglomerate the fly ash particles. This enhanced dispersion leads to more leaching of SiO₂ and Al₂O₃ from the source materials, thereby increasing the degree of geopolymerization. Mixtures with 0.1% CFs showed less intensity increase in the 1200-950 cm⁻¹ band compared to higher CF contents Nuaklong et al., (2021) as shown in figure 23.

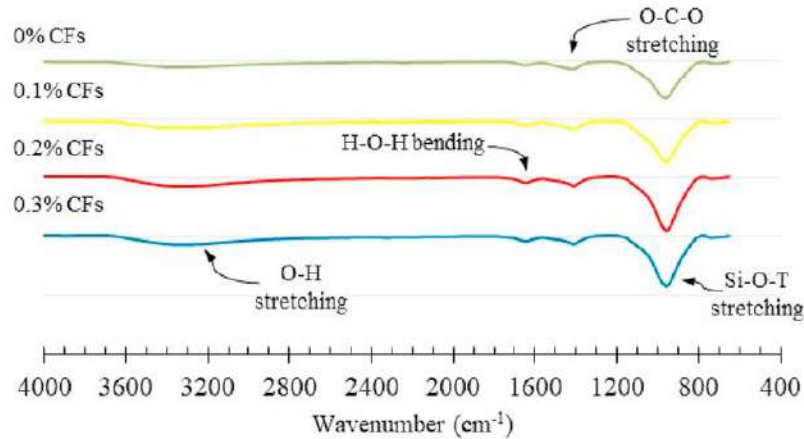


Figure 23. FTIR spectra of geopolymer paste with different micro-carbon fibre contents.
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5. Conclusion

The study elucidates the evolution of lightweight aggregates and their vital role in sustainable concrete construction. It outlines diverse methods for lightweight aggregate production, such as recycling waste materials and creating artificial aggregates, addressing sustainability needs. Additionally, it emphasizes the environmental advantages of geopolymer binders in lightweight concrete, potentially reducing the ecological footprint of Ordinary Portland Cement. Furthermore, it underscores the necessity for ongoing research on mix design and attributes of lightweight geopolymer concretes to enhance performance and encourage their extensive use in construction.

- Particle characteristics, aggregate types, and binder components significantly influence concrete workability. Fine aggregates like lightweight fine aggregates and smooth spherical aggregates enhance flowability and workability. Factors such as SS/SH ratio and GGBS content in the binder impact slump values.
- Alkaline content, binder composition, and curing conditions affect setting time. Higher NaOH concentrations generally extend setting times, enhancing workability but potentially impacting density and strength.
- Proper mix design and handling techniques can effectively minimize segregation and bleeding, ensuring uniform concrete quality and durability.

- Water absorption rates are influenced by aggregate types, GGBS content, and curing conditions. Denser structures with lower water absorption are achieved with higher alkalinity and GGBS additions.
- Flexural strength is influenced by aggregate types, binder components, and curing conditions. Lightweight aggregates and specific binder combinations can optimize flexural strength.
- Replacement of natural aggregate with recycled concrete aggregate and the addition of carbon fibers can affect split tensile strength positively, with optimal combinations enhancing performance.
- SEM Analysis: SEM reveals morphological changes and compositions, highlighting the impact of alkali activation and aggregate types on microstructure.
- XRD Analysis: XRD patterns demonstrate crystallographic changes and phase compositions, emphasizing the role of alkali activators and curing conditions.
- FTIR Analysis: FTIR spectra provide insights into molecular compositions, indicating water content, gel formation, and chemical reactions during geopolymerization.

Overall, geopolymer concrete technology offers promising advancements in achieving desired fresh and hardened properties, with further research focusing on optimizing mix designs, enhancing durability, and ensuring sustainable construction practices.

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Declarations

Competing interests: The authors declare that there is no conflict of interest regarding the publication of this paper.

Ethics Approval and Consent to Participate: The survey research directed has received ethical clearance from the ethics committee of the Graphic Era (Deemed to be University), Dehradun, Uttarakhand-248002, India. All respondents provided consent to participate in the research.

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